

AD-A189 638

CALCULATING DEPLETION REGION CARRIER CONCENTRATIONS
WITH CAPACITANCE-VOLT... (U) AIR FORCE INST OF TECH
WRIGHT-PATTERSON AFB OH SCHOOL OF ENGI... G H BAINER

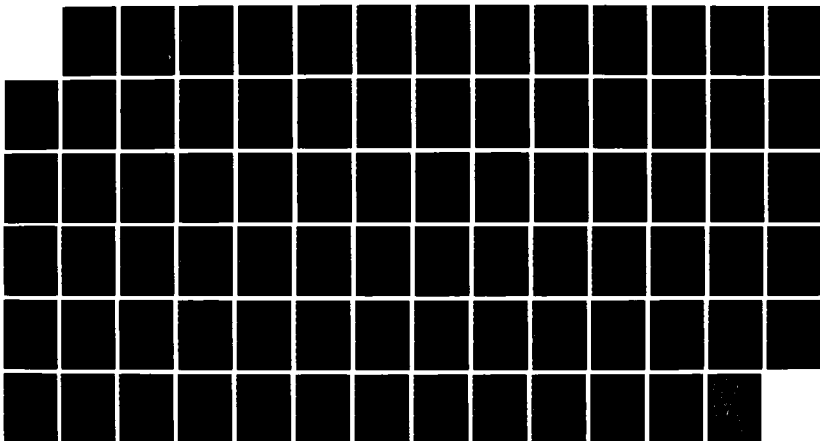
1/1

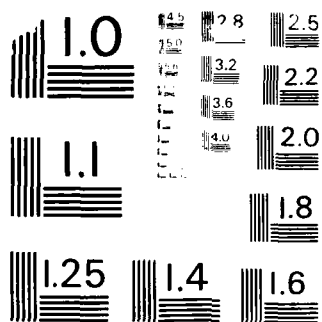
UNCLASSIFIED

DEC 87 AFIT/DEP/ENP/87D-8

F/8 20/12

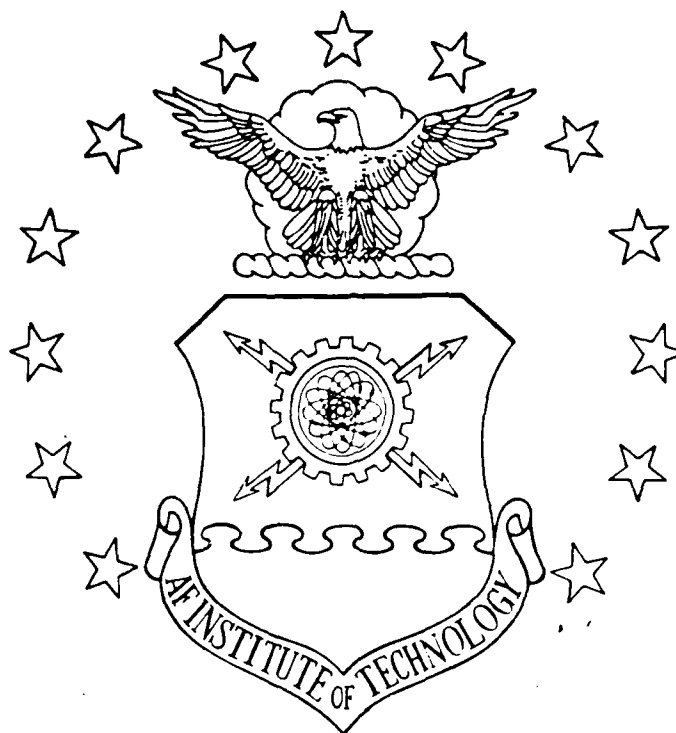
NL





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

AD-A189 630



CALCULATING DEPLETION REGION CARRIER
CONCENTRATIONS WITH CAPACITANCE-VOLTAGE
MEASUREMENTS AND ETCHING

THESIS

Gordon H. Gainer, Jr.
Captain, USAF

AFIT/GEP/ENP/87D-8

DTIC
ELECTE
MAR 03 1988
S
ce
E
D

DEPARTMENT OF THE AIR FORCE
AIR UNIVERSITY

AIR FORCE INSTITUTE OF TECHNOLOGY

Wright-Patterson Air Force Base, Ohio

This document has been approved
for public release and sale; its
distribution is unlimited.

88 3 01 043

O

DTIC
COPY
INSPECTED
1

[illegible]

2

Approved for Public Release; Distribution Unlimited

AFIT/GEP/ENP/87D-8

CALCULATING DEPLETION REGION CARRIER CONCENTRATIONS WITH
CAPACITANCE-VOLTAGE MEASUREMENTS AND ETCHING

THESIS

Presented to the Faculty of the School of Engineering
of the Air Force Institute of Technology

Air University

In Partial Fulfillment of the
Requirements for the Degree of
Masters of Science in Engineering Physics

Gordon H. Gainer, Jr., B.S.

Captain, USAF

December 1987

Approved for Public Release; Distribution Unlimited

Preface

The purpose of this study was to find a method of measuring the concentrations of charge carriers in n-type semiconductors within the initial depletion region. This method was to use capacitance-voltage measurements and the etching of layers from the semiconductor surface. All the necessary lab work was carried out at the Avionics Laboratory.

I wish to express great appreciation to several people of the Avionics Laboratory who helped me a great deal, such as Lt David Elsaesser, Capt Michael Sopko, Ben Carroll, Robert Neidhard, Michael Curtis, Mary Harshbarger, and Sgt James Foster. I wish also to express thanks to Dr. Y.K. Yeo, my thesis chairman.

Gordon H. Gainer, Jr.

Table of Contents

	Page
Preface	ii
List of Figures	iv
Abstract	vii
I. Introduction	1
Thesis Objective and Scope	3
Sequence of Presentation	3
II. Background	4
Ion Implantation	4
Lindhard, Sharff, and Schiott (LSS) Theory	5
Depletion Region of Metal-Semiconductor Contacts	7
Capacitance-Voltage Profiling	12
III. Experiments	16
Sample Preparation	16
C-V Measurements and Etching	17
IV. Theory	21
Charge Density Moment Method	21
Voltage Second Derivative Method	29
Voltage First Derivative Method	31
V. Computer Programs	35
VI. Results and Discussion	39
Results for Ideal C-V Data	39
Results for Experimental C-V Data	40
VII. Conclusions and Recommendations	63
Conclusions	63
Recommendations	64
Bibliography	66
Vita	68

List of Figures

Figure	Page
1. LSS Theoretical Ion Depth Profile	6
2. Ion Beam Orientation to Prevent Channeling	7
3. Energy Band Diagram for a Metal-Semiconductor Contact	8
4. The Kronig-Penney Periodic Potential with Asymmetric Potential at the Crystal Surface	11
5. The Formation of Localized States in the Forbidden Energy Region at the Surface of a 1-D Crystal	11
6. Depletion Region Due to a Metal-Semiconductor Contact with Applied Bias	13
7. Cross Section of Mercury Contacts	18
8. Potential Diagram of Metal-Semiconductor Contact	22
9. Abrupt Approximation of Depletion Region	24
10. Gradual Ending of Depletion Region	24
11. Etch Depths Across Carrier Profile	28
12. Potential Versus Etch Depth	30
13. An LSS Gaussian Carrier Distribution with a Range of $0.17\mu\text{m}$ and a Standard Deviation of $0.13\mu\text{m}$	42
14. Performance of the Charge Density Moment Method for the LSS Profile of Figure 13	43
15. Performance of the Voltage Second Derivative Method for the LSS Profile of Figure 13	44
16. Performance of the Voltage Second Derivative Method for a Linear Profile	45
17. Performance of the Voltage Second Derivative Method for the Parabolic Profile of Figure 18	46
18. A Parabolic Charge Carrier Profile	47

19. Performance of the Voltage Second Derivative Method When the Voltages of Every Other Etch Curve are Offset by 1 mV	48
20. Performance of the Voltage First Derivative Method for the LSS Profile of Figure 13	49
21. Performance of the Voltage First Derivative Method for a Linear Profile	50
22. Performance of the Voltage First Derivative Method for the Parabolic Profile of Figure 18	51
23. LSS Profile for Si-Implanted GaAs (Ion Dose: $1 \times 10^{13} \text{ cm}^{-2}$; Energy: 100 keV; Range: $.085 \mu\text{m}$; Standard Deviation: $.0442 \mu\text{m}$)	52
24. Performance of the Voltage First Derivative Method for Sample A311	53
25. Performance of the Voltage Second Derivative Method for Sample A311 (Averaged Over the First $0.2 \mu\text{m}$ of Each C-V Profile)	54
26. Performance of the Voltage Second Derivative Method for Sample A311 (Averaged Over the First $0.3 \mu\text{m}$ of Each C-V Profile)	55
27. Performance of the Voltage First Derivative Method for Sample A312	56
28. Performance of the Voltage Second Derivative Method for Sample A312 (Averaged Over the First $0.3 \mu\text{m}$ of Each C-V Profile)	57
29. Performance of the Voltage First Derivative Method for Sample S021	58
30. Performance of the Voltage Second Derivative Method for Sample S021 (Averaged Over the First $0.3 \mu\text{m}$ of Each C-V Profile)	59
31. Performance of the Voltage Second Derivative Method for Sample S021 (Averaged Over a Range of 0.1 to $0.3 \mu\text{m}$ From the Start of Each C-V Profile)	60
32. Performance of the Voltage First Derivative Method for Sample S022	61

33. Performance of the Voltage Second Derivative Method for Sample S022 (Averaged Over a Range of 0.03 to 0.13 μm From the Start of Each C-V Profile)	62
---	----

Abstract

Methods were developed for finding the charge carrier concentrations within the initial depletion region of n-type semiconductors. These methods combine the capacitance-voltage (C-V) technique with the etching of layers from the semiconductor surface. After each etch, the depletion region is made to end at the same location within the semiconductor. This location is used as a common reference and is arbitrarily chosen at a distance deep below the original unetched surface. For each etch depth, the voltage which extends the depletion region to the common reference distance is found. The voltage drop from an etch depth to the deeper common reference distance is the same as it would be if the semiconductor was not etched. This voltage drop is the sum of the applied voltage and the built-in potential. The built-in potential depends on the barrier potential at the semiconductor surface and the concentration at the common reference distance. Assuming the barrier potential is the same for each etch surface, the built-in potential is constant for each etch. Consequently, the applied bias voltage at each etch surface, can be treated as the potential at that etch depth. Then equations, such as Poisson's equation, can be used to find the carrier concentrations within the initial depletion region. These methods were successfully applied to ideal computer

generated C-V data as well as experimental C-V measurements of Si-implanted GaAs.

CALCULATING DEPLETION REGION CARRIER CONCENTRATIONS WITH CAPACITANCE-VOLTAGE MEASUREMENTS AND ETCHING

I. Introduction

Ion implantation of semiconductors is widely used in fabricating electronic and opto-electronic devices, such as FETs (field effect transistors), ICs (integrated circuits), and laser diodes. Si-implanted GaAs is widely used because of its high electron mobility and high electrical activation efficiency. Ion implantation gives higher precision and control of dopant profiles in semiconductors than epitaxial growth or thermal diffusion. Theoretically, a continuous variation of the fluence and energy of the incident ions can produce any desired dopant distribution (1:9). In addition, ion implantation can produce good uniformity of implants over large regions, as well as reproducibility from wafer to wafer (2:122). The electronic and opto-electronic device performances depend strongly upon the charge carrier depth profiles. For example, active layers in microwave FETs must be precisely controlled to depths of about 1 micron (3:14). Therefore, it is very important to be able to accurately measure the carrier profiles. These carrier profiles are usually obtained by the capacitance-voltage (C-V) method or by Hall-effect measurements. However, both methods have different advantages and limitations.

The differential Hall method can be used for both n- and p-type materials, but it is destructive. In this method, a Hall-effect measurement is made of the sheet carrier concentration, the electrically active carriers below the semiconductor surface per unit surface area. Then a thin layer is removed by chemical etching. Another Hall-effect measurement of the sheet carrier concentration can be used to find the carrier concentration in the removed layer. A problem not usually taken into account in differential Hall profiling is that a surface depletion region, produced by the filling of acceptor-type surface electronic states, causes the measured profile to be shifted from the true profile and contracted. However, a surface depletion correction can be made to the measured apparent Hall profiles (4:5070-5075).

The C-V method uses a reversed biased Schottky barrier on the semiconductor to create a variable depletion width, which can be found from its capacitance. The density of carriers at the edge of the depletion width can be found from the differential change of capacitance with bias voltage. The C-V method is nondestructive. However, the C-V method does not give a profile within the initial depletion width at zero bias voltage, and this depletion width often is 0.2 μm . Also, the C-V method can be practically applied only to n-type materials.

Thesis Objective and Scope

The objective of this thesis was to develop a method of calculating the carrier concentrations within the initial depletion region of semiconductors by combining C-V measurements with etching. The method was to be tested on Si-implanted GaAs. The GaAs samples used were <100> oriented and usually Cr-doped during crystal growth. The samples had been ion implanted at room temperature at an ion energy of 100 or 200 keV. The ion dose was 8×10^{12} or 1×10^{13} cm^{-2} . The samples were annealed at 800 or 850 °C for 15 minutes.

Sequence of Presentation

Chapter II provides background information on ion implantation and ion range statistics. Chapter II also reviews the theoretical basis of the C-V method and the cause of the initial depletion region. Chapter III describes the Si-implanted GaAs sample preparation and C-V measurements. Chapter IV discusses the theory of the methods developed for finding the depletion region concentrations, starting with Poisson's equation. Chapter V describes the computer programs developed to analyze and implement the methods. Chapter VI shows and discusses the performance of the methods. Chapter VII presents the successful conclusions of this study and the recommendations for further study.

II. Background

Ion Implantation

The electrical and optical properties of a semiconductor material can be altered by doping -- adding impurities. The impurities can be added before the semiconductor crystallizes from the liquid state or by diffusion or ion implantation afterwards. Chromium is often added during crystal growth to electrically compensate for other trace impurities. Thermal diffusion is used for uniform doping over large crystal sections. In ion implantation, the dopants penetrate into the semiconductor as an energetic ion beam. Ion implantation has the advantages of a wide choice of dopants, high accuracy in the dopant concentration and area of doping, a well defined dopant profile, slight lateral spreading, good reproducibility, and high yields at low cost. Ion implantation can also be used at low temperatures, and it can have good uniformity over large areas.

The ion bombardment has the disadvantage of causing radiation damage, such as vacancies, interstitials, clusters of point defects, dislocations and dislocation loops, and stacking faults, within the crystal structure. Also, some of the implanted ions do not go into substitutional lattice sites to become electrically active. These problems can be mostly corrected by annealing the crystal. At the high

annealing temperatures (800 - 1000 °C), dopant and substrate atoms can diffuse out of the crystal. This is prevented by encapsulating the crystal surface before annealing.

Lindhard, Sharff, and Schiott (LSS) Theory

In ion implantation, the dopant ions suffer collisions with the substrate nuclei and electrons before stopping. The LSS theory takes into account the electronic and nuclear stopping powers to calculate the penetration depth. The penetration depth depends on the initial kinetic energy of the incident ion, the atomic number and atomic mass of the incident ion and substrate atoms, the temperature, etc. Lindhard, Sharff, and Schiott used the Thomas-Fermi interatomic potential to calculate the ion energy loss due to nuclear collisions and the range or depth that ions would go below the surface of the substrate. Assuming a Gaussian range distribution, they also calculated a mean square fluctuation in this range (1:36-39). The ion implanted dopant concentration is then given by

$$N(x_p) = \frac{\phi}{\sigma_p \sqrt{2\pi}} \text{EXP} \left[\frac{-(x_p - R_p)^2}{2\sigma_p^2} \right] \quad (2.1)$$

where $N(x_p)$ is the dopant concentration at a depth x_p measured along the ion beam direction, ϕ is the ion beam fluence, and σ_p is the standard deviation in the projected range R_p . This is illustrated in Figure 1. Gibbons et al (5) developed a computer program to calculate the range and standard deviation for various implanted ions and

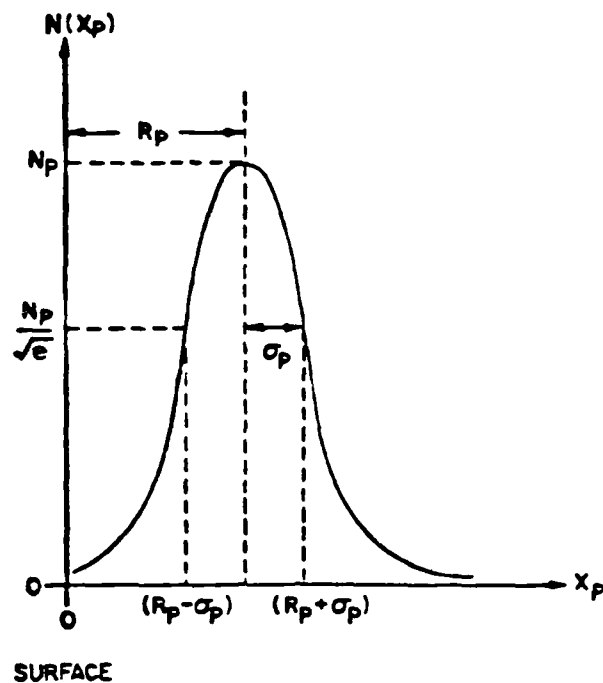


Figure 1. LSS Theoretical Ion Depth Profile

substrates. For example, Si ions with an energy of 100 keV have a projected range in GaAs of $0.085 \mu\text{m}$ and a standard deviation of $0.0442 \mu\text{m}$.

The Gaussian distribution is for the random collisions within an amorphous solid. However, in a crystal, the ions can be channeled down a major crystal axis and penetrate to much greater depths than in an amorphous solid. This channeling is prevented by aligning the ion beam at an angle to the major crystal axis, as shown in Figure 2 (6:13).

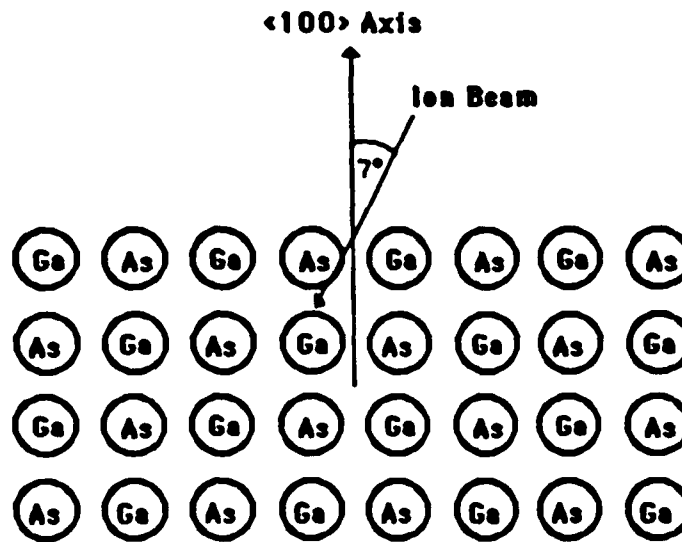


Figure 2. Ion Beam Orientation to Prevent Channelin

Depletion Region of Metal-Semiconductor Contacts

When a metal is brought into contact with an n-type semiconductor, the Fermi energy level E_F stays constant across the metal-semiconductor boundary as shown in the energy-band diagram of Figure 3. The conduction band minimum E_C of the semiconductor starts out level at a distance W from the metal and then rises to a barrier height $q\phi_B$ at the metal surface, where q is the electronic charge and ϕ_B is the barrier potential. The built-in potential V_{bi} is the difference between the potential at the metal surface and the potential at W . This built-in potential transfers electrons to the metal and ionizes donor atoms from the

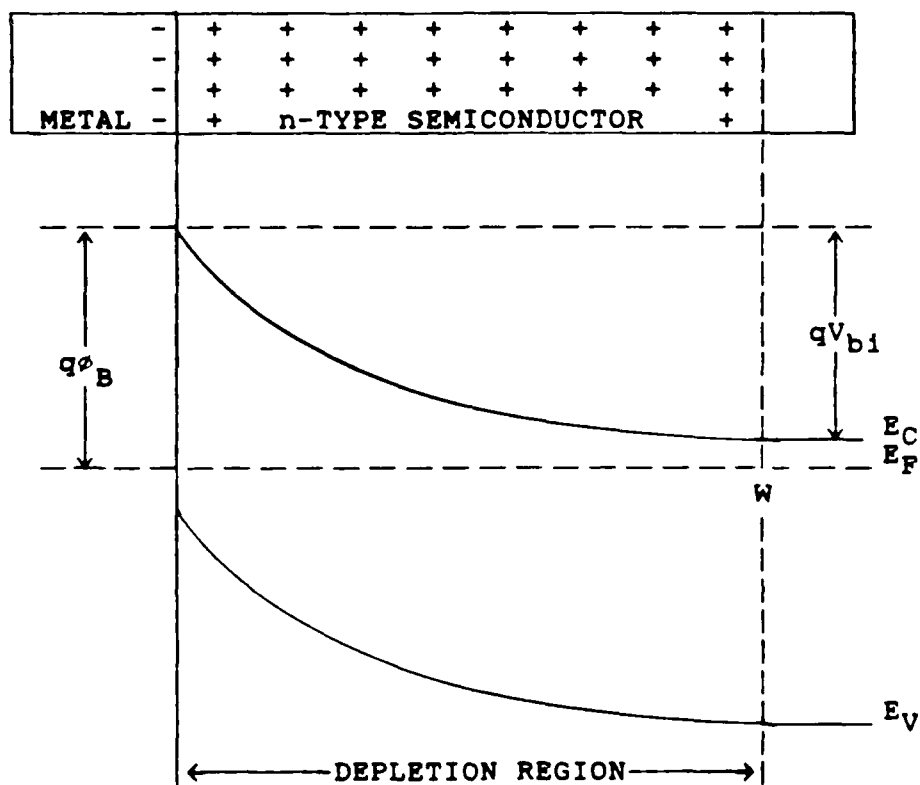


Figure 3. Energy Band Diagram for a Metal-Semiconductor Contact

metal surface to W , so W is called the depletion width.

Chandra et al (7:646) showed that the difference between the conduction band minimum and the Fermi level is given by

$$E_C - E_F = kT \ln[N_C/N(W)], \quad (2.2)$$

where k is the Boltzmann constant, T is the temperature, N_C is the density of states at the conduction band minimum, and $N(W)$ is the carrier concentration at the depletion width W . The carrier concentration is

$$N = N_D - N_A - n + p, \quad (2.3)$$

where N_D is the donor impurity concentration, N_A is the acceptor concentration, n is the electron concentration, and p is the hole concentration. The electron and hole concentrations are negligible where $N_D - N_A$ is high. The built-in potential is then

$$V_{bi} = \phi_B - (kT/q) \ln[N_C/(N_D - N_A)]. \quad (2.4)$$

According to Shottky (8:4), the built-in potential V_{bi} should be the difference between the work functions of the metal and the semiconductor, $V_{bi} = \phi_M - \phi_{SC}$. However, experiments showed that the rectification of metal-semiconductor contacts can be independent of the metal work function. In 1947, Bardeen (9:5) showed that the surface barrier potential ϕ_B is determined by surface states. The surface states produce the potential even without a metal contact. As explained by McKelvey (10:485), the Soviet physicist Tamm showed in 1932 that the surface states are

caused by the ending of a periodic potential, such as the Kronig-Penney square well potential, by a surface potential barrier, as shown in Figures 4 and 5. These additional states within the forbidden energy band of the Kronig-Penney model are the discrete allowed energy levels of wave functions localized near the surface. Shockley (11) calculated that there is one surface state for each surface atom. Surface states can also be created by impurity atoms, oxide layers, and surface imperfections. Treating the surface electronic states as unfilled orbitals or dangling bonds, Massies et al (12:64) experimentally observed the electron transition of a Ga 3d orbital to a dangling Ga bond on the (100) face of GaAs. The charging of the surface states causes the conduction band minimum and the valence band maximum to rise as they approach the surface, as shown in Figure 3. Henisch (13:184) explains that the Fermi level also rises to the surface, but when the semiconductor is brought to the metal, its Fermi level falls to equal the Fermi level of the metal. This creates an electric field between the metal and the semiconductor. If the density of surface states is large enough to take any additional charges that would be caused by the electric field, without much changing the Fermi level, then the space charge in the semiconductor is unaffected by the metal contact, and the barrier height potential is independent of the metal work function (13:184).

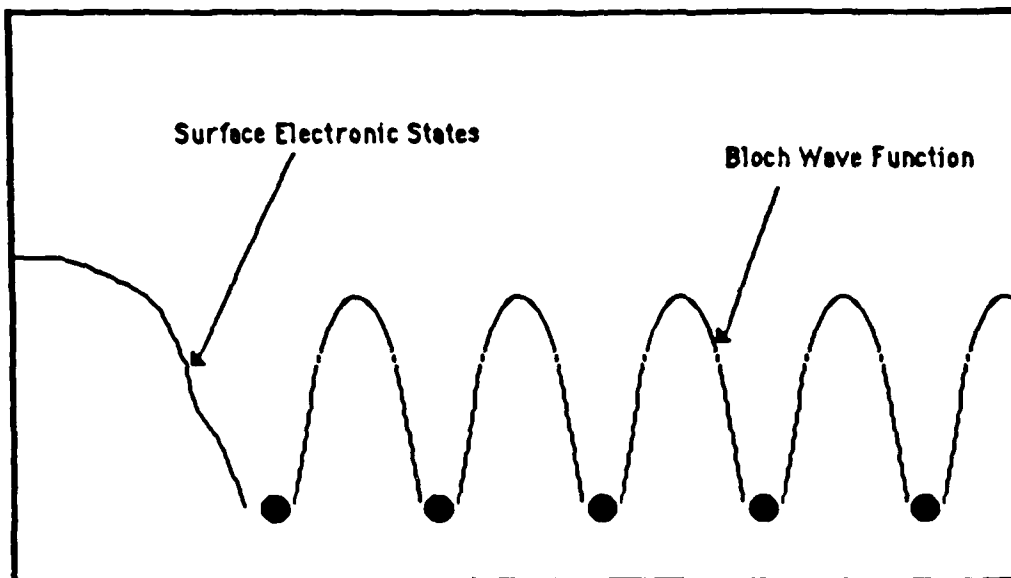


Figure 4. The Kronig-Penney Periodic Potential with Asymmetric Potential at the Crystal Surface

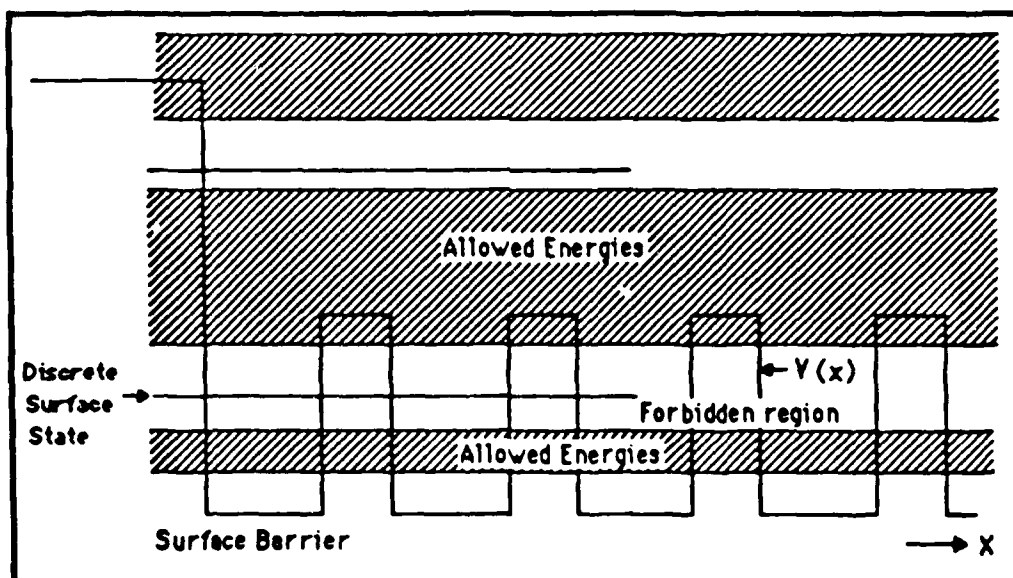


Figure 5. The Formation of Localized States in the Forbidden Energy Region at the Surface of a 1-D Crystal (10:486)

Capacitance-Voltage Profiling

When a metal and an n-type semiconductor are brought together, a space charge or depletion region is formed as shown in Figure 3. When a reverse bias voltage is applied to the contact, more electrons leave the semiconductor to the metal, extending the depletion width W deeper into the semiconductor as shown in Figure 6. In Figure 6, E_{FM} is the Fermi level in the metal, and E_{FS} is the Fermi level at the depth W within the semiconductor. The space charge region can be treated as a voltage dependent parallel plate capacitor, with capacitance

$$C = \epsilon A/W, \quad (2.5)$$

where C is the capacitance in Farads, ϵ is the permittivity of the material in Farads/cm, A is the area of the metal contact in cm^2 , and W is the depletion width in cm. As the applied bias voltage V increases, W increases, and C decreases.

In 1942, Schottky had the idea of using capacitance measurements to obtain dopant profiles (14). Copeland (15), Miller (16), and Nakhamanson (17) improved upon Schottky's idea to obtain the following equations for dopant profiles:

$$N(x) = \frac{-C^3}{\epsilon q A^2 (dC/dV)} \quad \text{at } x = \epsilon A/C, \quad (2.6)$$

where $N(x)$ is the carrier concentration at depth x below the semiconductor surface. The bias voltage is increased in small increments, and the capacitance is measured for each voltage to obtain dC/dV at each capacitance.

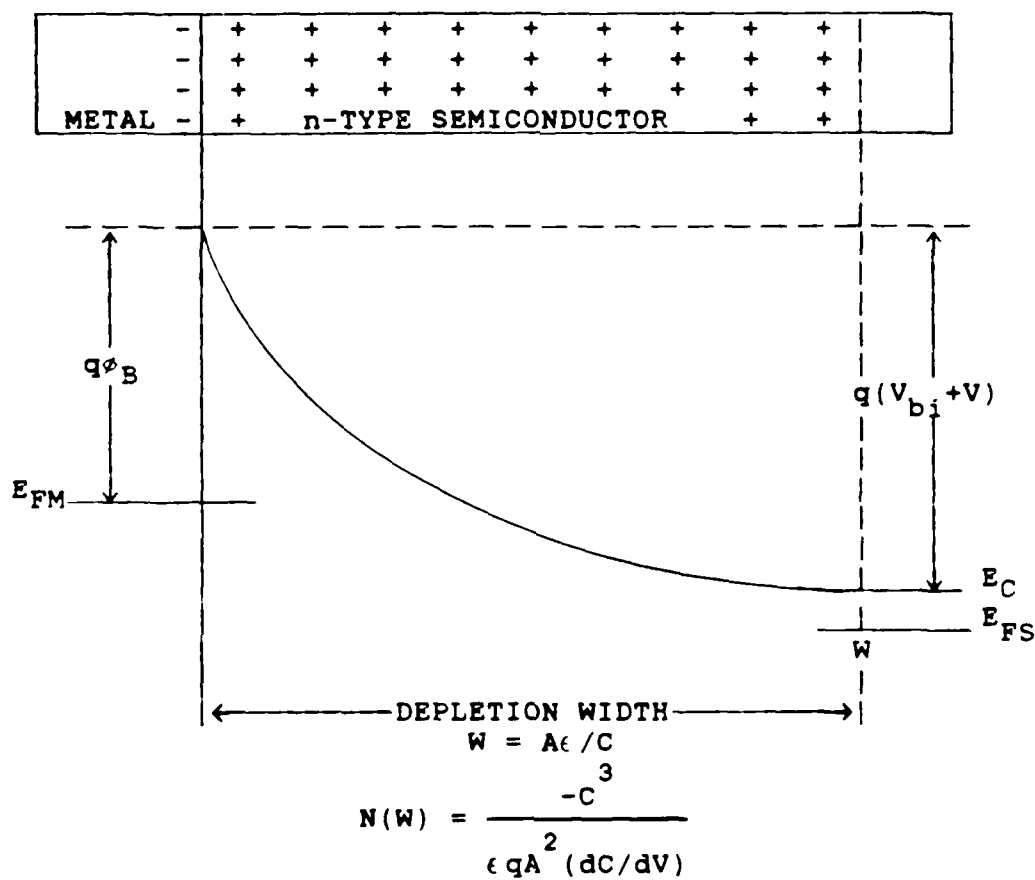


Figure 6. Depletion Region Due to a Metal-Semiconductor Contact with Applied Bias

To measure the capacitance, the bias voltages are actually superimposed upon an alternating voltage at frequency ω . The measured capacitance is

$$C' = C / (1 - \omega^2 r^2 C^2), \quad (2.7)$$

where C is the actual depletion layer capacitance, and r is a series resistance within the semiconductor (16:1106). $\omega r C$ is made small so that C' is approximately C . This is done by reducing the metal contact area to reduce C , requiring r to be small in the semiconductor, and making ω as small as possible without ruining the signal-to-noise ratio. The frequency must also be high compared to the relaxation times of traps in the semiconductor (16:1106). Traps hold on to electrons much longer than most dopant atoms and distort the measured profile. The best frequency for GaAs is usually about 1MHz.

This C-V profiling method has the advantages that 1) it measures only the electrically active impurity concentration, 2) it is completely automated, and 3) it is non-destructive. The C-V method has the disadvantages that 1) it cannot be used for concentrations above about 10^{18} cm^{-3} , because voltage breakdowns and current leaks occur, 2) it is practically restricted to n-type semiconductors, and 3) it cannot measure the concentrations within the initial depletion region, which occurs at zero applied bias voltage. The initial depletion region often ends $0.2 \mu\text{m}$ or deeper into the semiconductor. Applying a forward bias voltage would enable concentration measurements closer to the

semiconductor surface, except that at even small forward bias voltages a diffusion capacitance becomes too great (18:94). This paper explains a method of combining C-V measurements with the etching of layers from the semiconductor surface to measure the charge carrier concentrations within the initial depletion region.

III. Experiments

Sample Preparation

The samples used in this study were prepared and doped before the study began. The substrate materials used in the study were <100> oriented undoped or Cr-doped semi-insulating GaAs. The samples were originally cut into 1/4 inch squares from 2 inch circular wafers of the GaAs. Prior to implantation, each sample was cleaned with basic-H, de-ionized water, trichloroethylene, acetone, and methanol, and dried with blowing nitrogen gas. Then, the substrate was free-etched with an $\text{H}_2\text{SO}_4:30\%\text{H}_2\text{O}_2:\text{H}_2\text{O}$ solution in a 7:1:1 ratio by volume for 3 minutes. The samples were then ion implanted with Si at room temperature with an incident energy of 100 or 200 keV for a dose of 8×10^{12} or 1×10^{13} ions/cm². The ion beam was directed at 7 degrees off the <100> crystal axis to minimize ion channeling. After implantation, the samples were soaked in an HCl solution for 1 minute to remove a natural oxide layer which had grown since implantation. The samples were then immediately capped with a 1000 Å layer of Si_3N_4 using a pyrolytic deposition system. Next, the samples were annealed at 800 or 850 °C for 15 minutes in flowing hydrogen gas to activate the implanted ions. This produces high activation efficiencies, as shown by Kim (19:27), who achieved activation efficiencies of at least 80% for 6×10^{12} cm⁻²

Si-implants in GaAs. After annealing, the encapsulants were removed with a 48% hydrofluoric acid solution, which required about 5 minutes. Each half inch square sample was then cut into 4 quarter inch square samples.

C-V Measurements and Etching

A series of concentration profiles was measured for each Si implanted GaAs sample using the C-V technique. The samples were etched between the capacitance and voltage measurements to find the carrier concentrations within the initial depletion region of each sample. About ten etches were performed on each sample to acquire C-V data throughout the initial depletion region. The samples were cleaned before each set of capacitance and voltage measurements, because it was found that the cleaning could very much affect the measurements, especially if a sample was not cleaned for several days.

The C-V data was obtained using the Hewlett-Packard Model 4061 Semiconductor/Component Test System, which was controlled by a 9845B H-P Computer. A sample to be profiled was placed with the implanted face down onto a suction chuck as shown in Figure 7. The suction chuck has three ducts. One duct pulls the air out of a circular groove on the chuck creating a vacuum between the chuck and the sample. Actually, the samples were too small to cover the circular groove, so a sheet of plastic had to be placed over the test chuck and pressed down around the circular groove to obtain

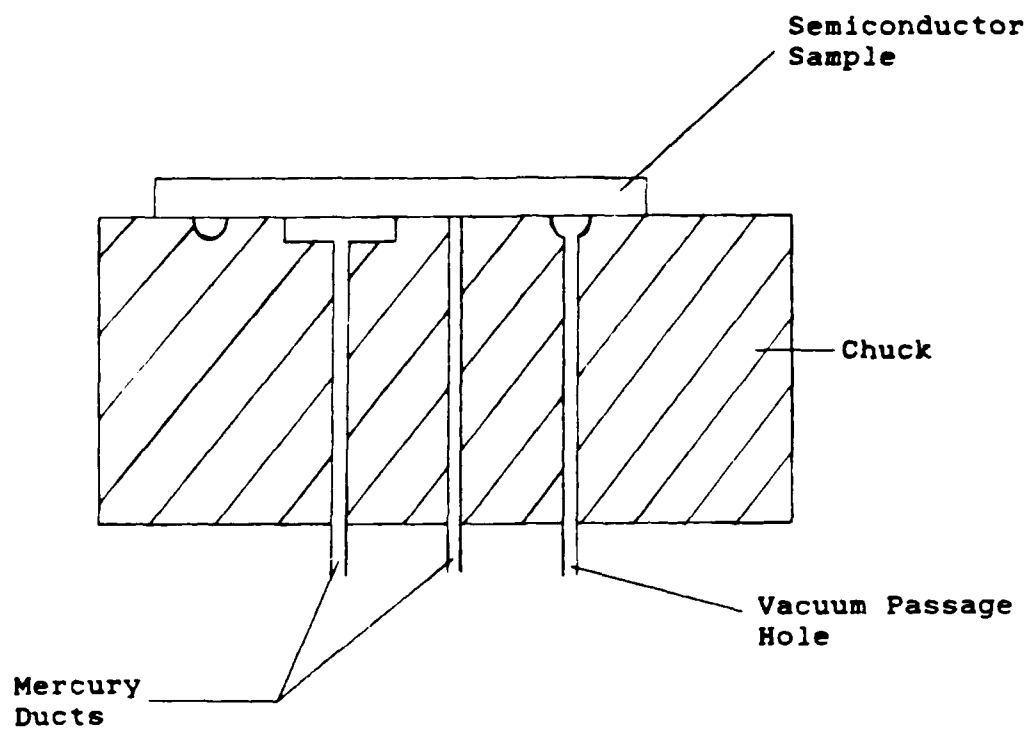


Figure 7. Cross Section of Mercury Contacts

a vacuum between the test chuck and the sample. This vacuum pulls the sample down to the chuck and pulls mercury up the other two ducts. The two mercury columns then make metal contacts with the test sample. One mercury duct has a much larger contact area, and it was connected to the high side of the bias supply. The smaller mercury duct was connected to the low side. Bias voltages from 0 to -5 or -10 volts were incrementally applied to the sample. The bias voltages were supplied by the Hewlett-Packard 4140B DC Voltage Source. The 4275A Multi-Frequency LCR Meter supplied a 0.01 V, 1 MHz test signal to measure the complex impedance and determine the capacitance of an assumed equivalent circuit. The circuit had the capacitance of the space charge region, or depletion region, in series with the resistance of the material between the two mercury contacts. The capacitance of the larger mercury contact area is much greater than that of the smaller mercury duct contact area, so the measured capacitance is approximately equal to the actual depletion region capacitance. C-V measurements were taken at two positions on each sample, and it was found that the measurements could change somewhat with the location of the mercury contact area. The C-V measurements were stored on tape in data files, which were transferred to the AFIT computer system.

Between the C-V measurements, etching was performed with an $\text{H}_2\text{SO}_4:30\%\text{H}_2\text{O}_2:\text{H}_2\text{O}$ solution in a 1:1:500 ratio by volume, at room temperature and with constant stirring.

This solution etched about 80 Å per minute. Alongside the sample to be etched, two control samples were also etched. The control samples were half coated with black wax, and the black wax was not removed until after the last etching. Since the control samples were not etched under the black wax, a step height could be measured on these samples as a total etched depth, and thus, the etch rate could be determined. The etched depth was measured using the Sloan-Dektak IIA Surface Profiling System.

IV. Theory

Three methods were developed for determining the charge carrier concentration within the initial depletion region. They are the Charge Density Moment Method, the Voltage Second Derivative Method, and the Voltage First Derivative Method. The Voltage Second Derivative Method is the best mathematically, but the Voltage First Derivative Method is much less sensitive to experimental error.

Charge Density Moment Method

When a metal is brought into contact with an n-type semiconductor under a reverse bias applied voltage V , the potential ψ varies with depth into the semiconductor as shown in Figure 8. The potential falls off steeply and then levels off at a distance x_W . ϕ_B is the barrier potential. E_C is the conduction band minimum at x_W , and E_{FS} is the Fermi energy level at x_W . q is the electronic charge. V_{bi} is the built-in potential. The depletion region extends from $x = 0$ to $x = x_W$. As seen by equation (2.4), the built-in potential depends on the endpoints $x = 0$ and $x = x_W$. The potential ψ is governed by Poisson's equation:

$$-\frac{d^2\psi}{dx^2} = \frac{\rho(x)}{\epsilon} = \frac{qN(x)}{\epsilon} = \frac{dE}{dx}, \quad (4.1)$$

where $\rho(x)$ is the charge density at x , ϵ is the permittivity of the semiconductor, $N(x)$ is the carrier concentration given by equation (2.3) at x , and E is the electric field.

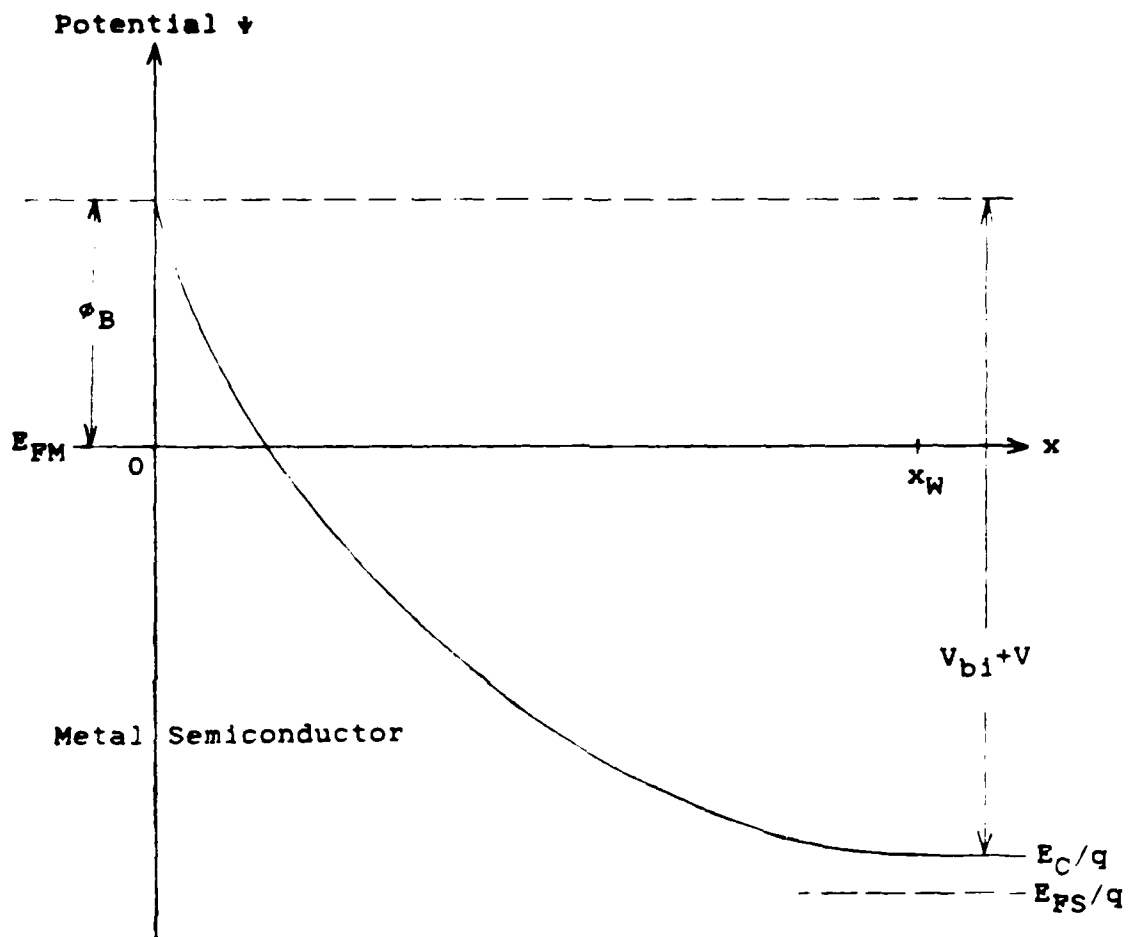


Figure 8. Potential Diagram of Metal-Semiconductor Contact

By integrating Poisson's equation once, the electric field is found to be

$$E(x) = \frac{q}{\epsilon} \int_x^{x_W} N(x) dx + E_W, \quad (4.2)$$

where E_W is the electric field at x_W (20:209). This is the same result that would be obtained using Gauss' Law, since the integral term contains the total charge per area from x to x_W . By integrating a second time, the voltage drop from the surface to x_W is shown to be

$$V + V_{bi} = \frac{q}{\epsilon} \int_0^{x_W} \int_x^{x_W} N(x) dx dx + x_W E_W, \quad (4.3)$$

where V is the applied reverse bias voltage required to extend the depletion region to x_W , and the reverse bias voltages are considered positive. Giacoletto (20:210) pointed out that this double integral can be integrated by parts to yield

$$V + V_{bi} = \frac{q}{\epsilon} \int_0^{x_W} x N(x) dx + x_W E_W, \quad (4.4)$$

which relates the applied voltage to a moment of the charge density. If the depletion region is assumed to end abruptly as shown in Figure 9, then E_W is zero, since there are no charges right of x_W . Actually, the depletion region ends gradually, as shown in Figure 10, due to an electron "tail" at x_W (18:74-77). The electron concentrations near x_W are usually considered small and the abrupt approximation applied, so that E_W is considered negligible (21:790). With the E_W term dropped off, the above equation is

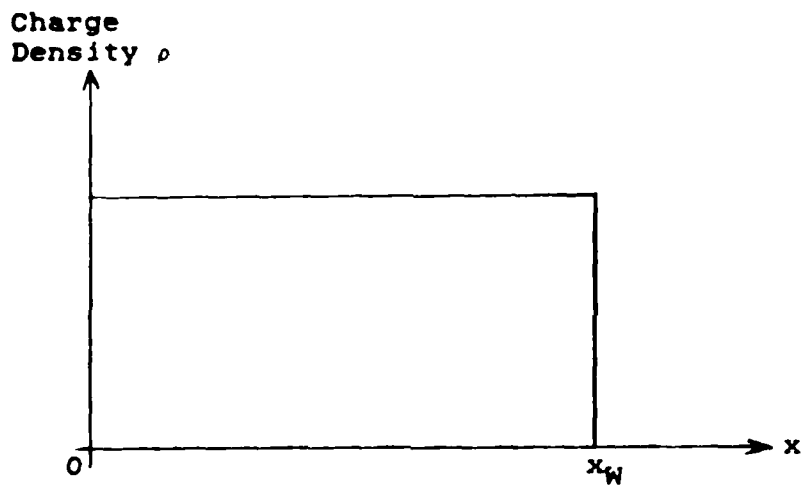


Figure 9. Abrupt Approximation of Depletion Region

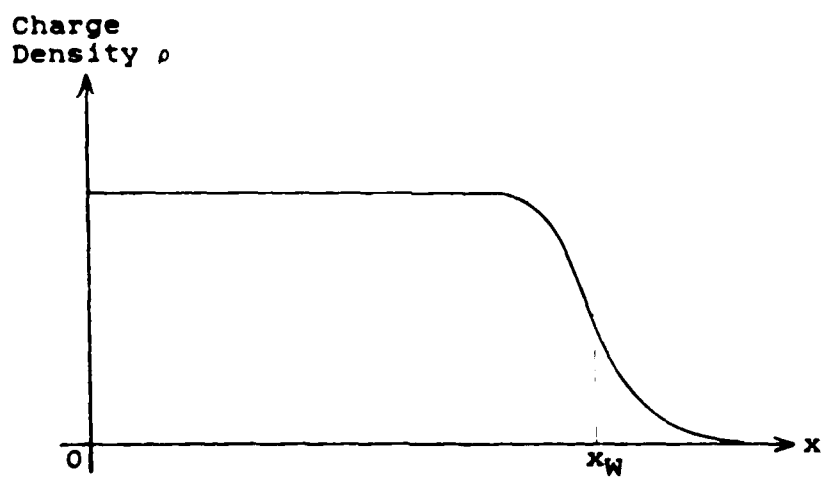


Figure 10. Gradual Ending of Depletion Region

$$V + V_{bi} = \frac{q}{\epsilon} \int_0^{x_W} xN(x)dx. \quad (4.5)$$

From this equation, it can be seen that even if one measures V , V_{bi} , and x_W , an infinite number of $N(x)$ profiles could give the same result. There is no unique $N(x)$ profile that satisfies equation (4.5).

Giacoletto (20:215) also showed that the voltage drop from a position x_0 to x_W is

$$\psi(x_0) - \psi(x_W) = \frac{q}{\epsilon} \int_{x_0}^{x_W} (x-x_0)N(x)dx + (x_W-x_0)E_W, \quad (4.6)$$

where x_0 is between 0 and x_W . If x_W is far from both $x=0$ and $x=x_0$, then E_W and the shape of the space charge region (as shown in Figure 10) should change very little with etching of the semiconductor between the surface and x_0 . Under these circumstances, it can be seen from equation (4.6), that the potential drop from x_0 to x_W is the same regardless of whether material has been etched away between 0 and x_0 . In that case,

$$V(x_0, x_W) + V_{bi}(x_0, x_W) = \psi(x_0) - \psi(x_W), \quad (4.7)$$

where $V(x_0, x_W)$ and $V_{bi}(x_0, x_W)$ are respectively the applied voltage and built-in potential when the depletion region extends from an etch depth of x_0 to x_W .

If one designates the i th etch thickness as t_i and the distance of the i th etched surface from the original unetched surface as T_i , then

$$T_i = \sum_{j=0}^i t_j \text{ and } T_0 = 0. \quad (4.8)$$

The potential difference between T_i and x_W is

$$V(T_i, x_W) + V_{bi}(T_i, x_W) = \frac{q}{\epsilon} \int_{T_i}^{x_W} (x - T_i) N(x) dx + (x_W - T_i) E_W(T_i, x_W), \quad (4.9)$$

where $E_W(T_i, x_W)$ is the electric field at x_W when the depletion region starts at the etch depth T_i , and x_W is given by

$$x_W = \epsilon A / C(T_i, x_W). \quad (4.10)$$

$C(T_i, x_W)$ is the capacitance measured when the applied bias voltage is $V(T_i, x_W)$. There are various ways equation (4.9) can be used to find the concentration $N(x)$ within the initial depletion region. The voltage drop from the etch depth T_{i-1} to x_W is

$$\begin{aligned} V(T_{i-1}, x_W) + V_{bi}(T_{i-1}, x_W) &= \frac{q}{\epsilon} \int_{T_{i-1}}^{x_W} (x - T_{i-1}) N(x) dx + \\ &+ (x_W - T_{i-1}) E_W(T_{i-1}, x_W). \end{aligned} \quad (4.11)$$

As shown by equation (2.4), the built-in potential V_{bi} depends on the etch surface barrier potential ϕ_B and the carrier concentration $N(x_W)$ at x_W . If one assumes that the surface barrier potential ϕ_B is the same for each etch depth, and if x_W is used as a common reference, then the built-in potentials are the same:

$$V_{bi}(T_i, x_W) = V_{bi}(T_{i-1}, x_W). \quad (4.12)$$

As described earlier, the electric field at x_W changes little with a change in the etch depth, especially if x_W is far from the etch surfaces. The electric field at x_W is usually considered as near zero anyway. Therefore, subtracting equation (4.9) from equation (4.11) yields

$$V(T_{i-1}, x_W) - V(T_i, x_W) = \frac{q}{\epsilon} \int_{T_{i-1}}^{x_W} (x - T_{i-1}) N(x) dx - \frac{q}{\epsilon} \int_{T_i}^{x_W} (x - T_i) N(x) dx, \quad (4.13)$$

which can be expressed as

$$\int_{T_{i-1}}^{T_i} (x - T_{i-1}) N(x) dx = \frac{\epsilon}{q} [V(T_{i-1}, x_W) - V(T_i, x_W)] - (T_i - T_{i-1}) \int_{T_i}^{x_W} N(x) dx. \quad (4.14)$$

With the Nth etch depth T_N as the distance to the end of the initial depletion region of the original unetched surface, as shown in Figure 11, then

$$\int_{T_{N-1}}^{T_N} (x - T_{N-1}) N(x) dx = \frac{\epsilon}{q} [V(T_{N-1}, x_W) - V(T_N, x_W)] - (T_N - T_{N-1}) \int_{T_N}^{x_W} N(x) dx. \quad (4.15)$$

The quantities on the right side of equation (4.15) are all measurable or known. If the etch thicknesses are small, the concentration $N(x)$ can be treated as uniform or constant between T_{N-1} and T_N . Using t_N for the Nth etch thickness

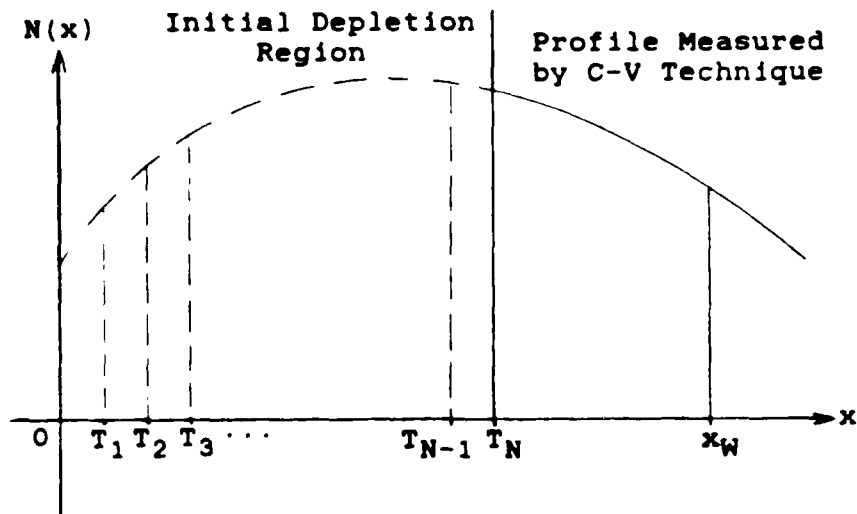


Figure 11. Etch Depths Across Carrier Profile

between the etch depths, the integral on the left side can then be evaluated and the equation solved for N to give

$$N \cong \frac{2}{t_N^2} \left\{ \frac{\epsilon}{q} [V(T_{N-1}, x_W) - V(T_N, x_W)] - t_N \int_{T_N}^{x_W} N(x) dx \right\}, \quad (4.16)$$

and this value of N can be assigned to the midpoint of the two etch depths:

$$x = \frac{T_{N-1} + T_N}{2}. \quad (4.17)$$

With $N(x)$ known between T_{N-1} and T_N , the same method can then be applied to find $N(x)$ between T_{N-2} and T_{N-1} . This method can be repeatedly applied working backward to the original unetched surface.

Since this method treats the concentration as uniform between each pair of etch depths, its values of the concentrations will be slightly different from the true values. If the value calculated for the concentration within one etch layer is smaller than the true value, the calculated value in the next etch layer will compensate by being higher than its true value. Thus, the concentrations calculated by this method oscillate about the true profile. In this case, a best fit curve should be obtained. Another disadvantage of this method is that it cannot be applied until after etching to the end of the initial depletion region.

Voltage Second Derivative Method

As explained in the previous section, the basic shape of the space charge region should stay nearly constant from one etch depth to the next, if x_W is far from the etch depths and the etch thickness is small. Then, equation (4.7) can be used, and

$$V(T_i, x_W) = \psi(T_i) - \psi(x_W) - V_{bi}(T_i, x_W). \quad (4.18)$$

Furthermore, if x_W is used as a common reference distance for each etch depth, $\psi(x_W)$ and $V_{bi}(T_i, x_W)$ can be treated as constants. Then, the applied voltage is the potential difference above $\psi(x_W) + V_{bi}$, as shown in Figure 12. Consequently, equation (4.1) can be used to find the

concentration:

$$N(x) = \frac{-\epsilon}{q} \frac{d^2V}{dx^2} . \quad (4.19)$$

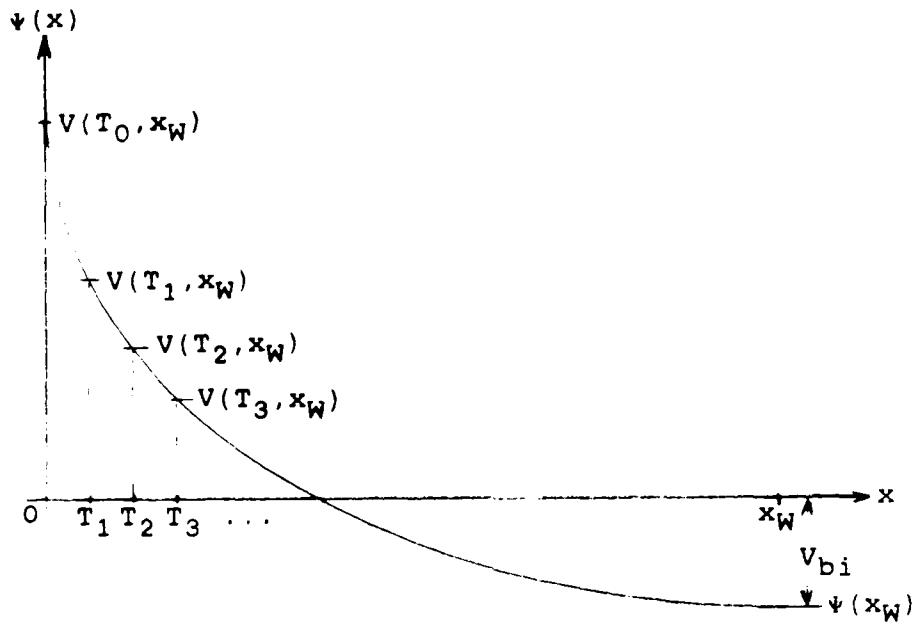


Figure 12. Potential Versus Etch Depth

Considering the reverse bias voltages as positive, and expressing the voltage second derivative in terms of etch thicknesses and etch depths, the concentration is

$$N \cong \frac{2\epsilon}{q(t_i + t_{i+1})} \left[\frac{V(T_{i-1}, x_W) - V(T_i, x_W)}{t_i} - \frac{V(T_i, x_W) - V(T_{i+1}, x_W)}{t_{i+1}} \right] , \quad (4.20)$$

and this value of N can be assigned to the midpoint of the two etch layers:

$$x = \frac{T_{i-1} + T_{i+1}}{2} . \quad (4.21)$$

It can be mathematically shown that equation (4.20) gives a value of the concentration which is between the minimum and maximum values of $N(x)$ in the range between T_{i-1} and T_{i+1} , if the measured voltages and thicknesses are exact. However, since equation (4.20) is based on a second derivative, it is very sensitive to experimental error. Much higher accuracy can be obtained by smoothing the curve of the voltage first derivative and then taking the derivative of this curve to obtain the voltage second derivative. Further accuracy can be obtained by using small etch thicknesses and averaging $N(x)$ over a range of x_W 's. This Voltage Second Derivative Method is much simpler than the Charge Density Moment Method and can be immediately applied after the first two etches (three, counting the zeroth etch).

Voltage First Derivative Method

By Gauss' Law, the electric field at a depth within the semiconductor is proportional to the charge per area past that depth:

$$E(x) = \frac{q}{\epsilon} \int_x^{\infty} N(x) dx. \quad (4.22)$$

If one assumes that most of the charge is within the depletion width, then

$$E(x) = \frac{q}{\epsilon} \int_x^{x_W} N(x) dx, \quad (4.23)$$

where x_W is the end of the depletion region. The average value of $N(x)$ between x and x_W is

$$N_{av}(x, x_W) = \frac{\int_x^{x_W} N(x) dx}{(x_W - x)} = \frac{\epsilon}{q} \frac{E(x)}{(x_W - x)} . \quad (4.24)$$

As illustrated in Figure 12, the derivative of the potential is the derivative of the applied voltage which extends the depletion region from an etch depth x to x_W . The electric field at x is then

$$E(x) = - \frac{d\psi}{dx} = - \frac{dV}{dx} . \quad (4.25)$$

In terms of etch depths and thicknesses, the electric field is

$$E \left[x = \frac{T_i + T_{i+1}}{2} \right] \cong - \frac{[V(T_{i+1}, x_W) - V(T_i, x_W)]}{t_{i+1}} . \quad (4.26)$$

Substituting the electric field of equation (4.26) into equation (4.24) gives

$$N_{av} \left(\frac{T_i + T_{i+1}}{2} , x_W \right) \cong \frac{\epsilon}{q} \frac{[V(T_i, x_W) - V(T_{i+1}, x_W)]}{t_{i+1} \left[x_W - \frac{T_i + T_{i+1}}{2} \right]} . \quad (4.27)$$

This average value of N can be assigned to the midpoint of the range of its average:

$$x = \left[\frac{T_i + T_{i+1}}{2} + x_W \right] / 2 = (T_i + \frac{t_{i+1}}{2} + x_W) / 2 . \quad (4.28)$$

This is the Voltage First Derivative Method. It is a crude

approximation, and it approximates the concentrations only in the second half of the depletion region, but it is much less sensitive to experimental error than the Voltage Second Derivative Method. Also, the value of N throughout the initial depletion region can be calculated more precisely by using the Voltage First Derivative Method as a first step of the Voltage Second Derivative Method, as described below.

The value of N between etch layers can be determined by using sheet-carrier concentrations. The sheet-carrier concentration $N_s(x_0, x_W)$ is the total charge carriers per area from x_0 to x_W . The sheet-carrier concentration is given by

$$N_s(x_0, x_W) = N_{av}(x_0, x_W)(x_W - x_0) . \quad (4.29)$$

The concentration between depths x_0 and x_1 can be determined from

$$N \left(x = \frac{x_0 + x_1}{2} \right) \cong N_{av}(x_0, x_1) = \frac{N_s(x_0, x_W) - N_s(x_1, x_W)}{(x_1 - x_0)} . \quad (4.30)$$

By using equations (4.29) and (4.30), the value of N between etch layers can be obtained from

$$N \left(x = \frac{T_{i-1} + T_{i+1}}{2} \right) \cong \frac{N_{av} \left(\frac{T_{i-1} + T_i}{2}, x_w \right) \left(x_w - \frac{T_{i-1} + T_i}{2} \right) - N_{av} \left(\frac{T_i + T_{i+1}}{2}, x_w \right) \left(x_w - \frac{T_i + T_{i+1}}{2} \right)}{(T_{i+1} - T_{i-1})/2} \quad (4.31)$$

By using equation (4.27) for the average concentrations in equation (4.31), equation (4.20) is obtained, so the Voltage Second Derivative Method is based on the Voltage First Derivative Method. Therefore, inaccuracies and experimental error in the Voltage First Derivative Method appear much larger in the Voltage Second Derivative Method. If the average concentrations calculated using equation (4.27) are curve fit or smoothed, then good results can be obtained using equation (4.31).

V. Computer Programs

Computer programs were written to implement the methods developed in the previous section and use capacitance-voltage data to calculate the carrier concentrations within the initial depletion region. To better analyze these methods, files of ideal capacitance-voltage data were computer generated for various dopant distributions. C-V equations (2.6) could be applied in reverse to create the ideal data, but it was found that the C-V equations can be derived from the differential form of equation (4.5):

$$dV = \frac{q}{\epsilon} xN(x)dx \quad (5.1)$$

by using

$$C = \epsilon A/x \quad (5.2)$$

These equations (5.1) and (5.2) were used to generate the ideal C-V data. Since equations (5.1) and (5.2) are the same type of equations used in developing the methods of finding the initial depletion region concentrations, the methods could not be proven using the ideal computer generated C-V data. However, it is assuring that the methods are based on the same assumptions as the regular C-V technique, and the ideal data could still be used in analyzing the methods and the effects of experimental error. The capacitances after the *i*th etch were easily calculated as

$$C(i,j) = \epsilon A / (x_j - T_1), \quad (5.3)$$

where $C(i,j)$ is the j th capacitance after the i th etch and x_j is the j th distance from the original unetched surface.

$$x_j = T_1 + jh, \quad (5.4)$$

where h is a small distance interval. Similar to equation (5.1), the voltages were determined from

$$V(i,j) - V(i,j-1) = \frac{-q}{\epsilon} jh \frac{[N(x_j) + N(x_{j-h})]}{2} h, \quad (5.5)$$

where $V(i,j)$ is the j th total voltage after the i th etch, considering reverse bias voltages as negative. A constant built-in potential of 0.8 V was assumed throughout the calculations for the ideal C-V data, so the zeroth voltage was set at 0.8: $V(i,0) = 0.8$. The voltage increments were added to this starting voltage to obtain the applied bias voltages. The voltage and capacitance pairs with voltages less than or equal to 0, were stored in a data file for the i th etch. Usually, 11 data files were made for 10 etches, 100 Å each.

To calculate the concentrations from the data files by the regular C-V technique, the finite difference form of equation (2.6) was used:

$$N(x) = \frac{[V(i,j-1) - V(i,j)]}{\epsilon q A^2 [C(i,j) - C(i,j-1)]} \left[\frac{C(i,j) + C(i,j-1)}{2} \right]^3, \quad (5.6)$$

where

$$x = T_i + \frac{2\epsilon A}{[C(i,j) + C(i,j-1)]} . \quad (5.7)$$

As expected, the profiles calculated by this C-V technique, for the different etches, overlapped exactly for the ideal C-V data. For the experimental data, the profiles for the different etches overlapped only approximately, as shown in Figures 26 to 37.

The computer programs used to find the depletion region concentrations all required a measure of $V(T_i, x_W)$, the applied voltage necessary to extend the depletion region from the etch depth T_i to the common reference distance x_W . The distances from the original unetched surface to the edge of the depletion region were given by

$$D(i,j) = T_i + \frac{\epsilon A}{C(i,j)} . \quad (5.8)$$

Thus, for each $V(i,j)$, there was an associated distance $D(i,j)$. $V(T_i, x_W)$ could then be found through linear or spline interpolation between these distances.

For the Voltage Second Derivative Method, the concentration at each depth was averaged over a range of common reference distances x_W . These ranges were chosen where the C-V profiles overlapped best for the different etches. However, the Voltage First Derivative Method is most accurate when the common reference distance is chosen as close as possible to the original unetched surface, since this narrows the distances over which the concentrations are

averaged. For this reason, each point calculated by the Voltage First Derivative Method was calculated using only one common reference distance, which was as close as possible to the original unetched surface.

VI. Results and Discussion

Results for Ideal C-V Data

Figure 14 shows the performance of the Charge Density Moment Method for the ideal C-V data of the LSS Gaussian distribution shown in Figure 13. The calculated concentrations in the initial depletion region oscillated more than expected about the true curve. The amount of oscillation varied with the choice of the common reference distance x_w . This was probably because of inaccuracies in the voltage interpolations caused by too large of a step size in generating the ideal data. The Charge Density Moment Method cannot be applied until after etching to the end of the initial depletion region. Also, this method required an integration to find the area under the profile from the edge of the depletion region to the common reference distance. Slight differences in this area could very much affect the results of this method, and the profiles obtained using the regular C-V technique did not overlap well. For these reasons and because of the oscillations about the true profile, this method was not attempted on experimental data.

The Voltage Second Derivative Method worked very well on the ideal data, as shown for the LSS profile of Figure 15, the linear profile of Figure 16, and the parabolic profile of Figure 17. The original LSS profile is shown in

Figure 12, and the original parabolic profile of Figure 17 is shown in Figure 18. In these figures, the first data point calculated by the regular C-V technique after each etch is labeled with the number of the etch. Figure 19 shows the results of the Voltage Second Derivative Method when the voltages of every other etch are purposely offset by 1 mV. This was done to show how sensitive the method is to experimental inaccuracies.

The Voltage First Derivative Method worked much better than expected, as shown for the LSS, linear, and parabolic distributions in Figures 20, 21, and 22, respectively. The concentrations calculated by this method start at the midpoint of the initial depletion region and extend outside the depletion region, almost overlapping the profiles calculated by the regular C-V technique.

Results for Experimental C-V Data

As explained at the end of Section IV, the Voltage Second Derivative Method is based on the Voltage First Derivative Method, so inaccuracies in the latter show up much greater in the former. The results of these two methods should be viewed together. For comparison with these methods, an LSS distribution is shown in Figure 23. The LSS curve is for Si implanted into GaAs at an energy of 100 keV and a dose of $1 \times 10^{13} \text{ cm}^{-2}$, which was usually used in this study. The results of the two methods are shown in Figures 24 - 33. The Voltage First Derivative Method gave

concentrations starting at the midpoint of the initial depletion region and then approximately overlapping the C-V profiles just as demonstrated in Figure 20 for ideal data. However, the curves calculated by this method were much more jagged for the experimental data. This jaggedness can be seen as fluctuations about a true profile, so a smooth curve can be drawn through these fluctuations. By using the data of a smooth curve with equation (4.31), which is another form of the Voltage Second Derivative Method, good results can be obtained for the concentrations throughout the initial depletion region. In this way the Voltage First Derivative Method can be used as a first step of the Voltage Second Derivative Method. When the Voltage Second Derivative Method is applied alone, the results can be erratic, as shown in Figures 25, 26, 28, 30, 31, and 33. A different common reference distance was used for each point calculated by the Voltage First Derivative Method, but the same common reference distance must be used for each point, when the first derivative method is used as a first step in the second derivative method. This was tried, but the calculated data points were too few and the fluctuations too large to confidently draw a smooth curve through the fluctuations.

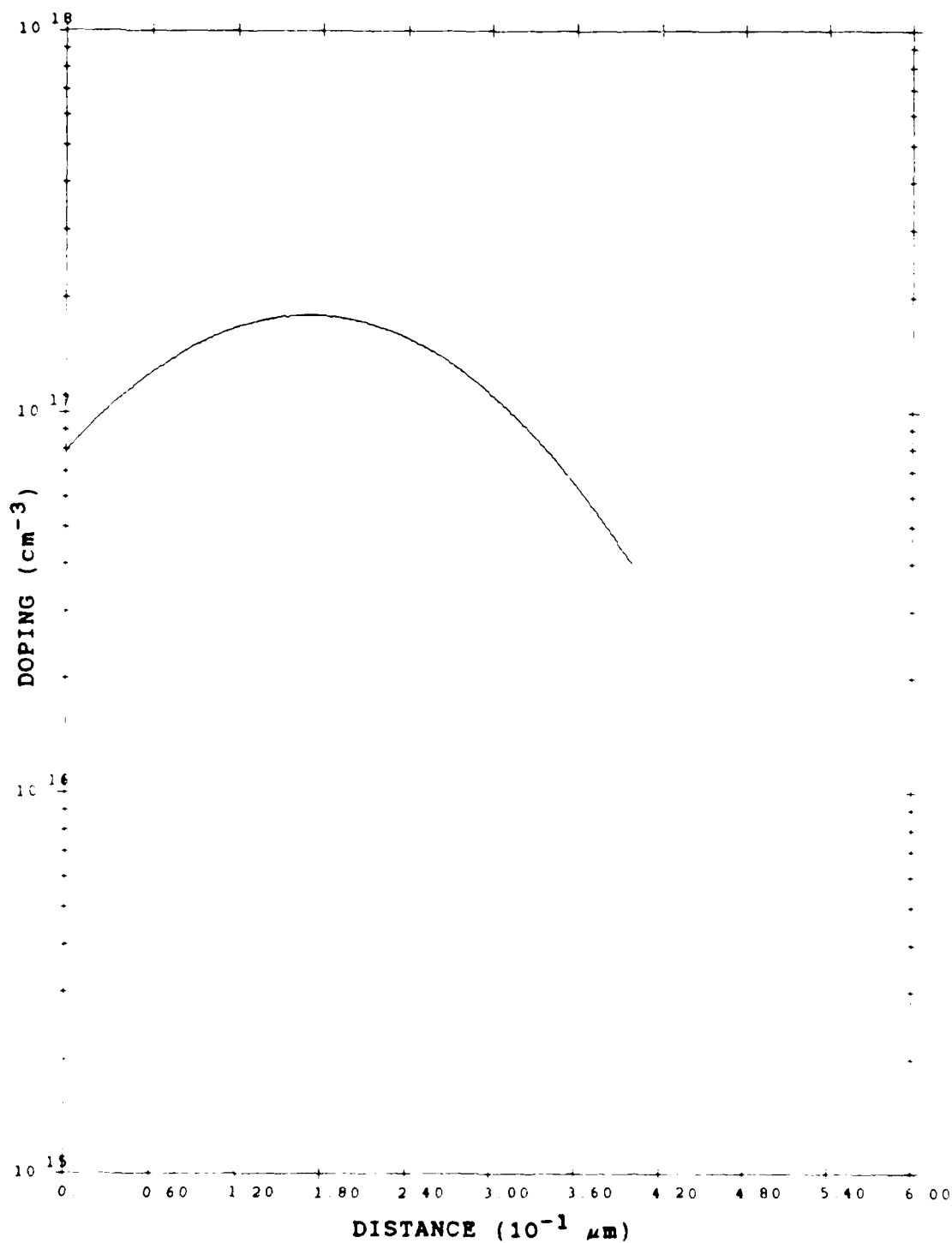


Figure 13. An LSS Gaussian Carrier Distribution with a Range of 0.17μm and a Standard Deviation of 0.13μm

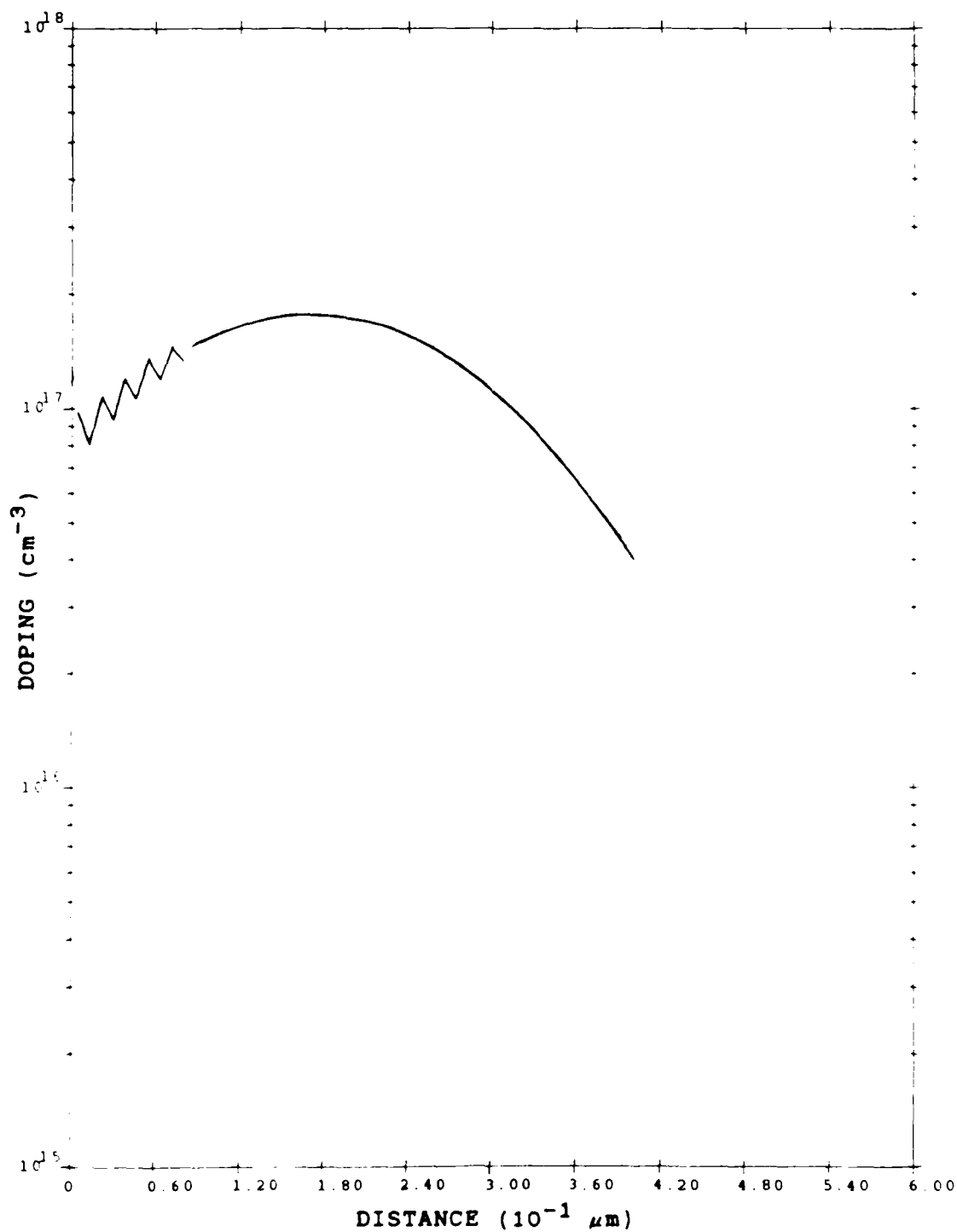


Figure 14. Performance of the Charge Density Moment Method for the LSS Profile of Figure 13

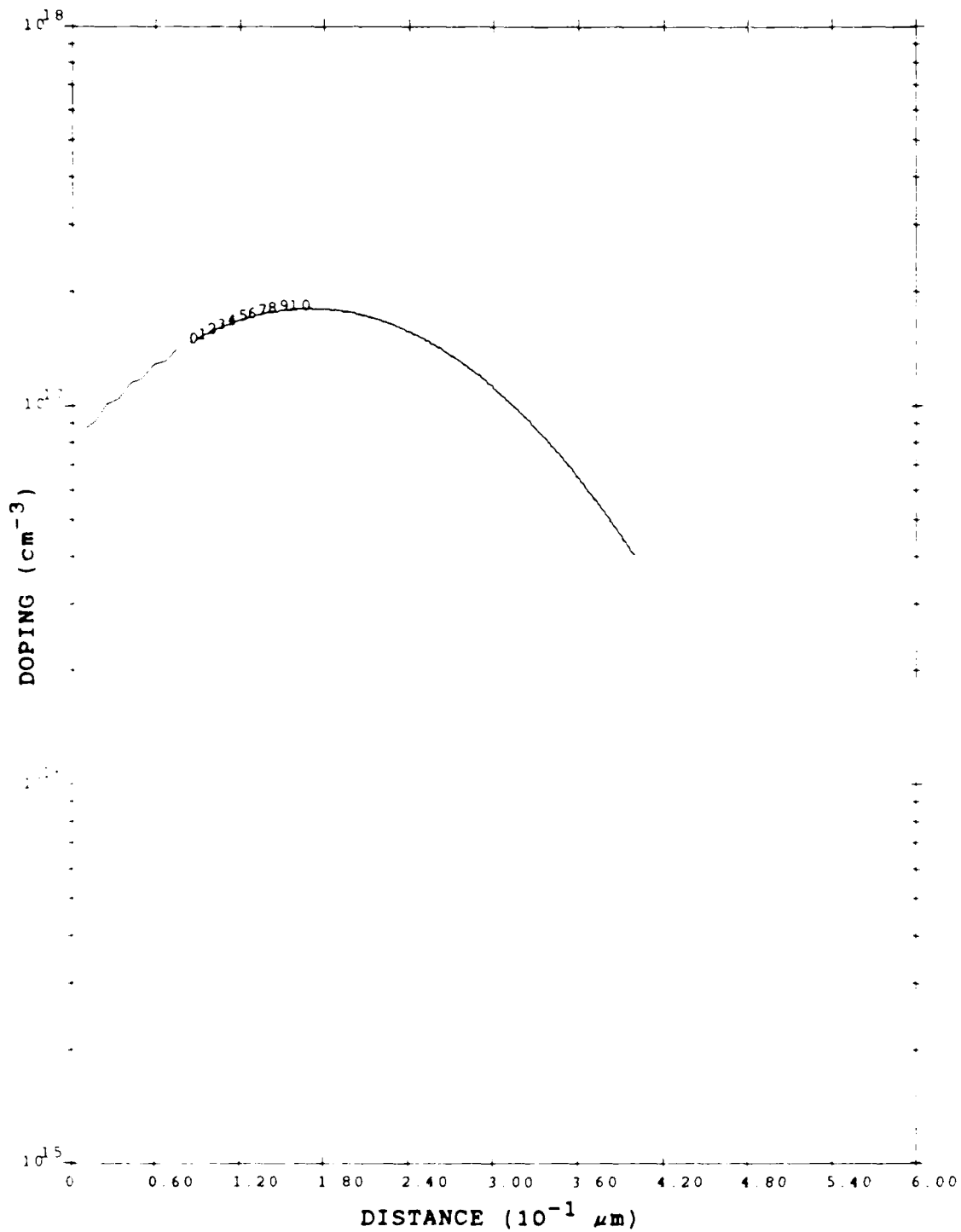


Figure 15. Performance of the Voltage Second Derivative Method for the LSS Profile of Figure 13

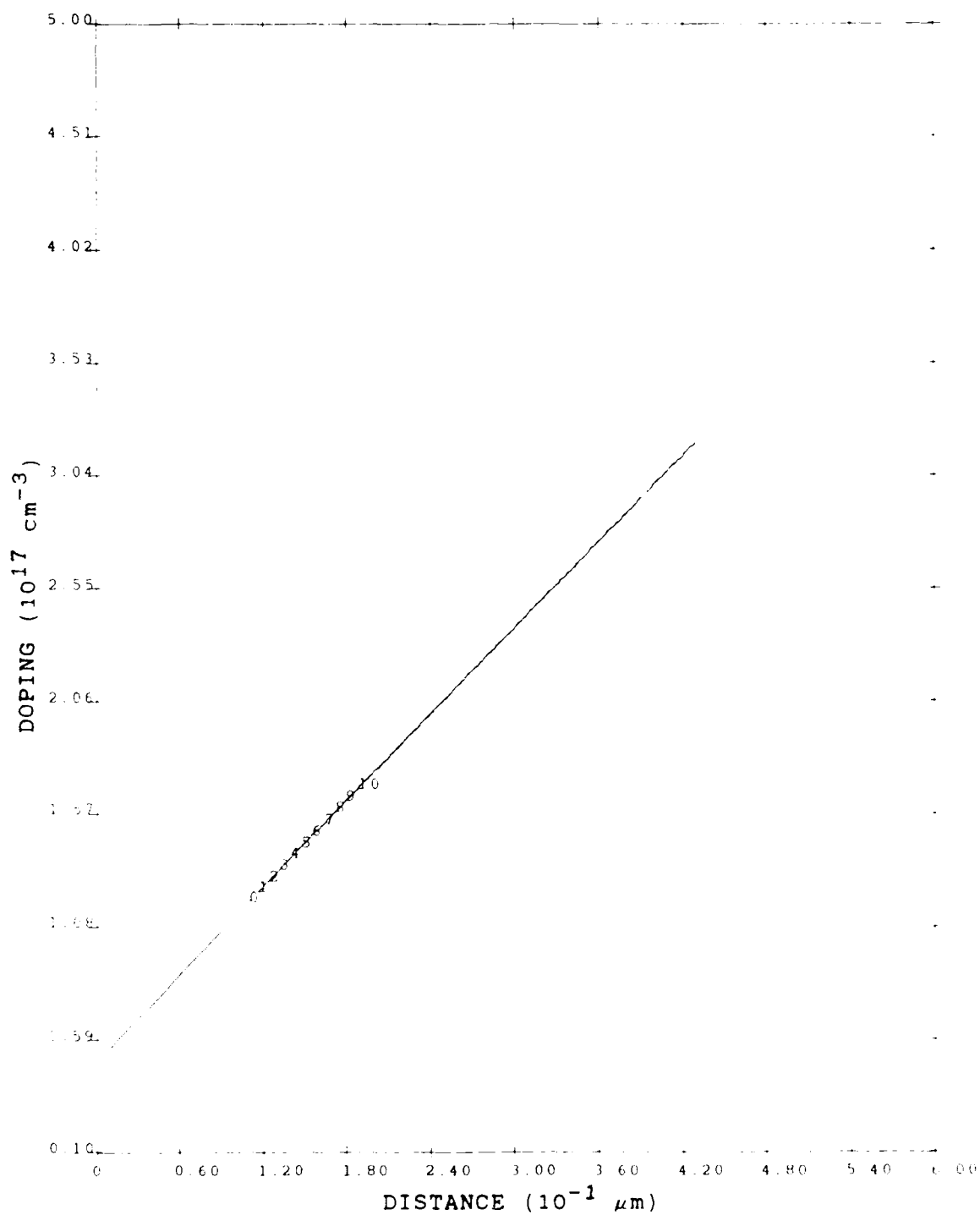


Figure 16. Performance of The Voltage Second Derivative Method for a Linear Profile

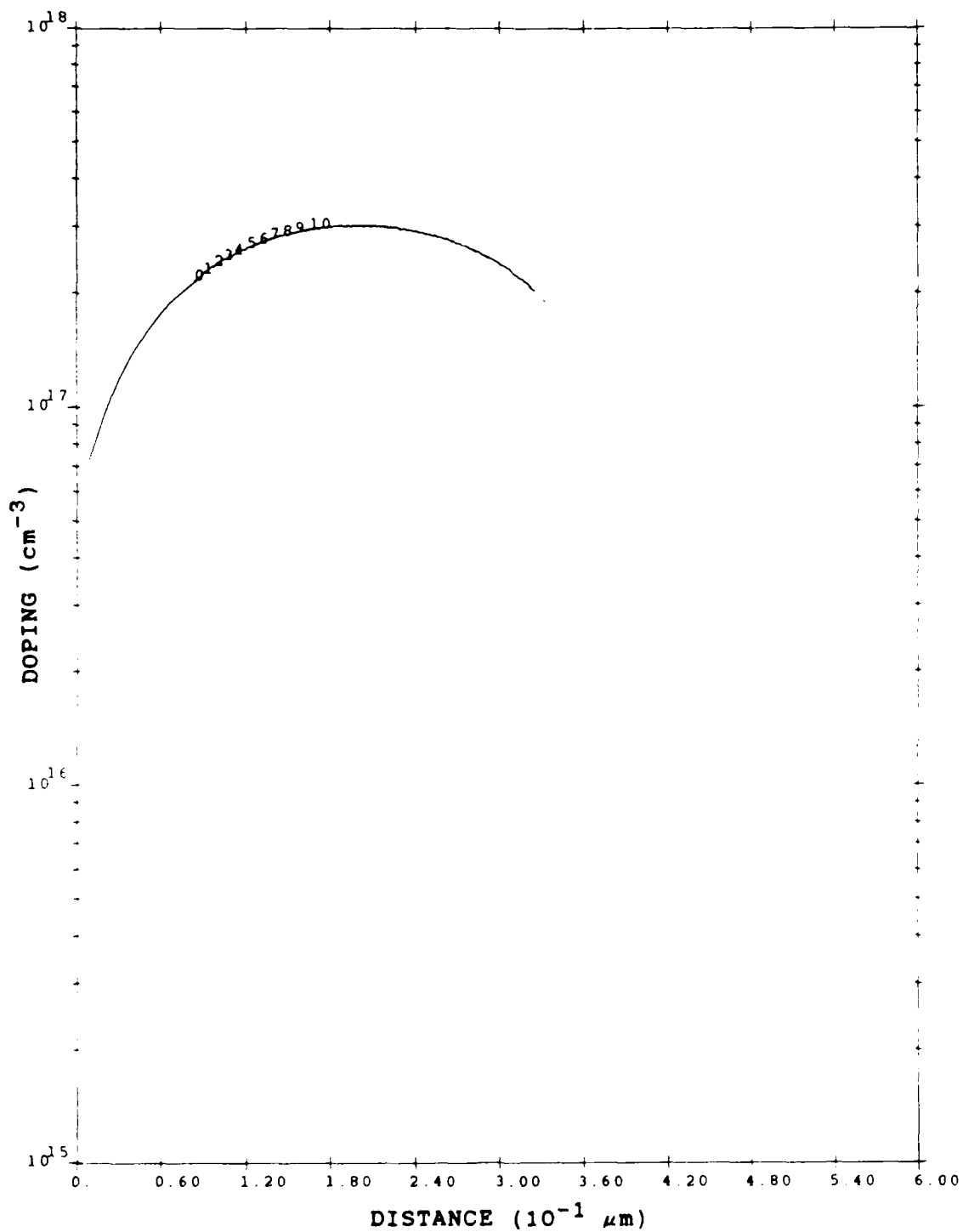


Figure 17. Performance of the Voltage Second Derivative Method for the Parabolic Profile of Figure 18

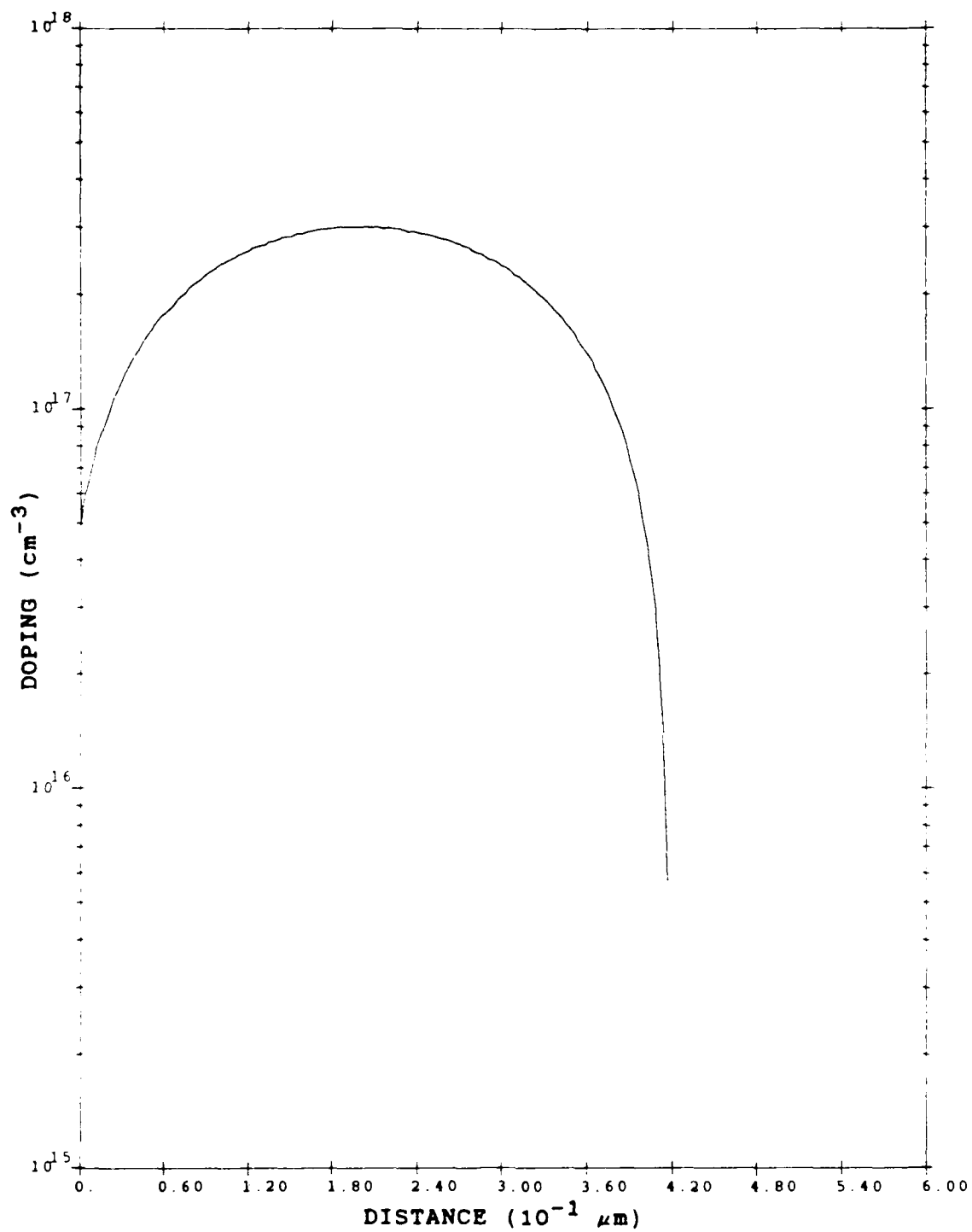


Figure 18. A Parabolic Charge Carrier Profile

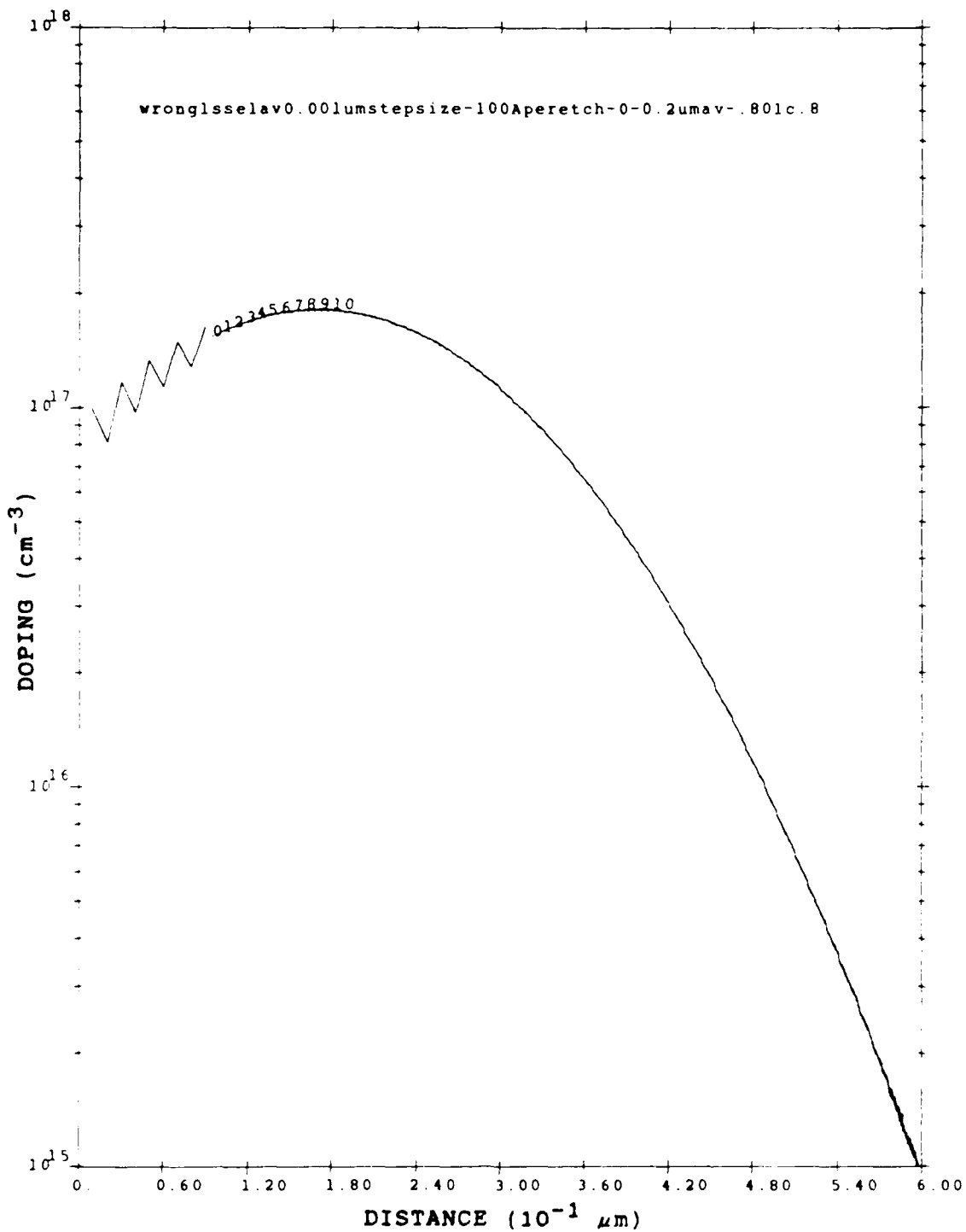


Figure 19. Performance of the Voltage Second Derivative Method When the Voltages of Every Other Etch Curve are Offset by 1 mV

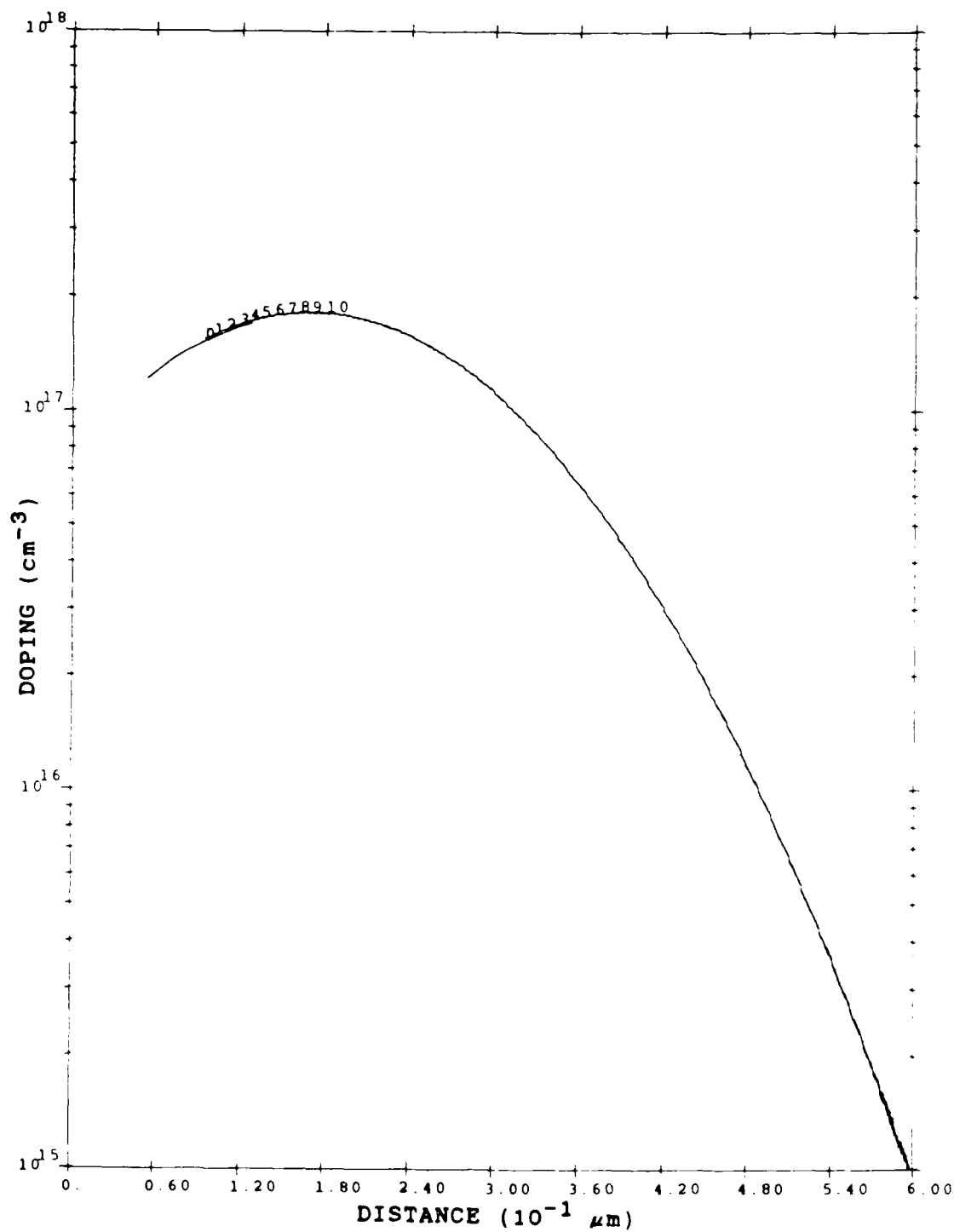


Figure 20. Performance of the Voltage First Derivative Method for the LSS Profile of Figure 13

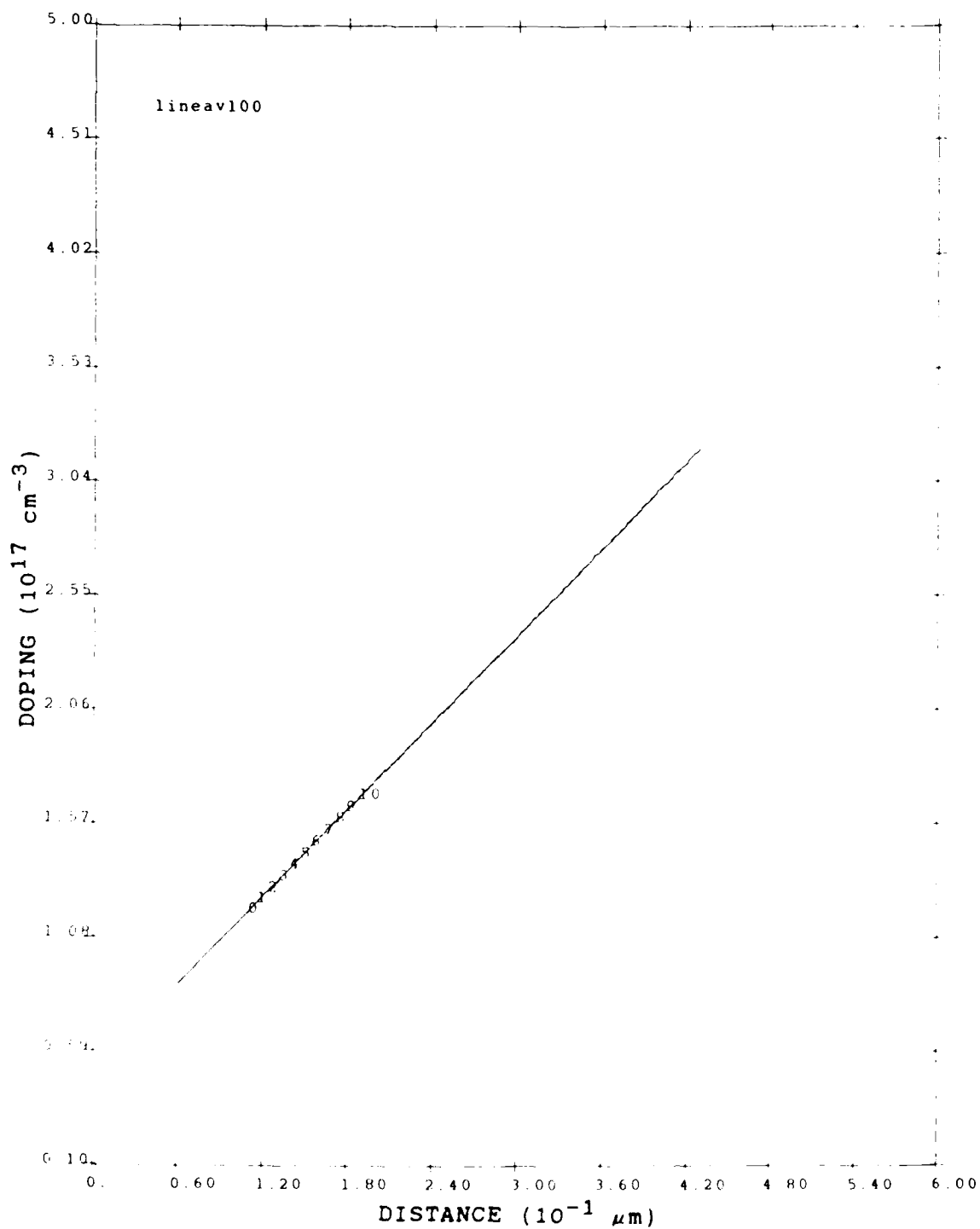


Figure 21. Performance of the Voltage First Derivative Method for a Linear Profile

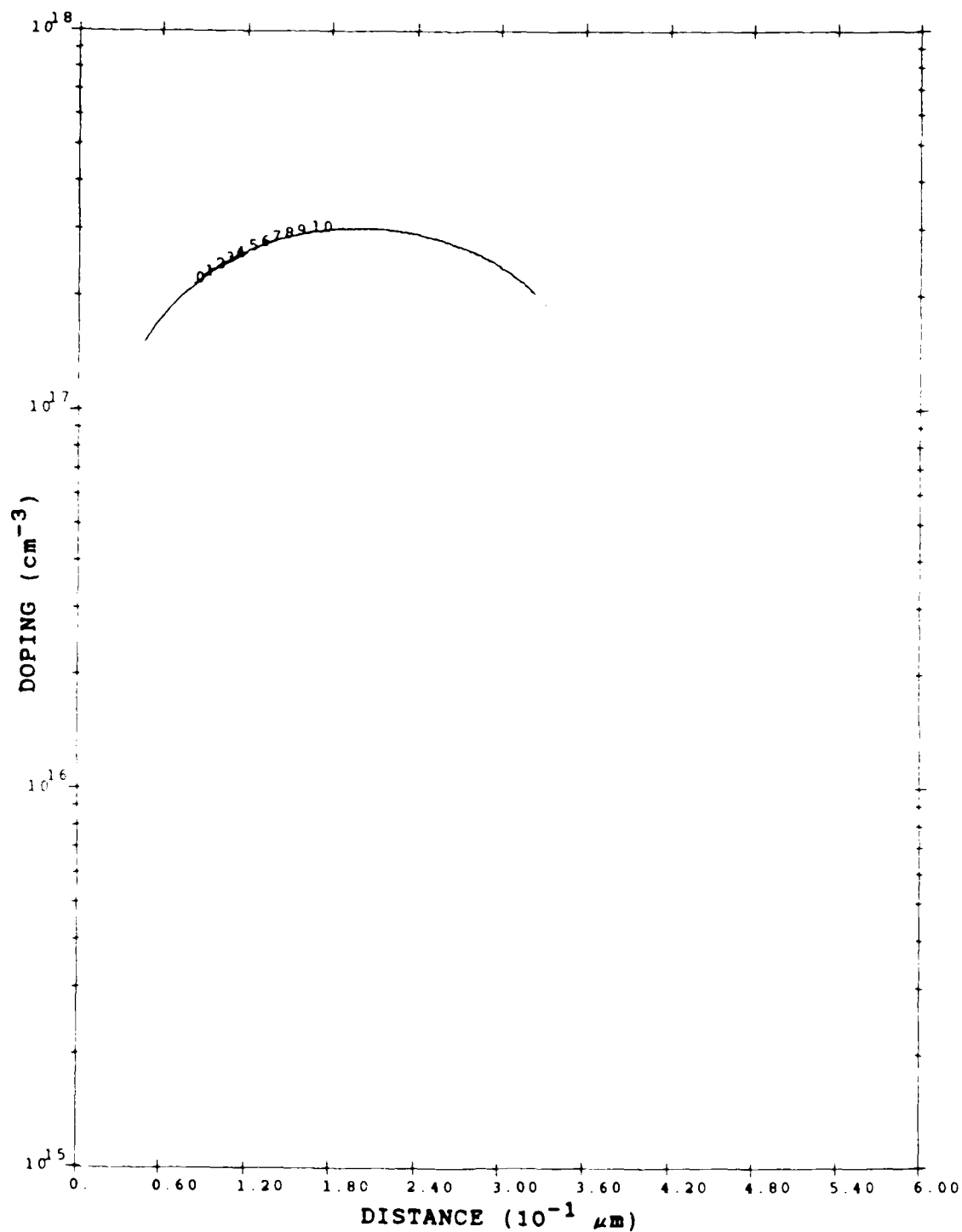


Figure 22. Performance of the Voltage First Derivative Method for the Parabolic Profile of Figure 18

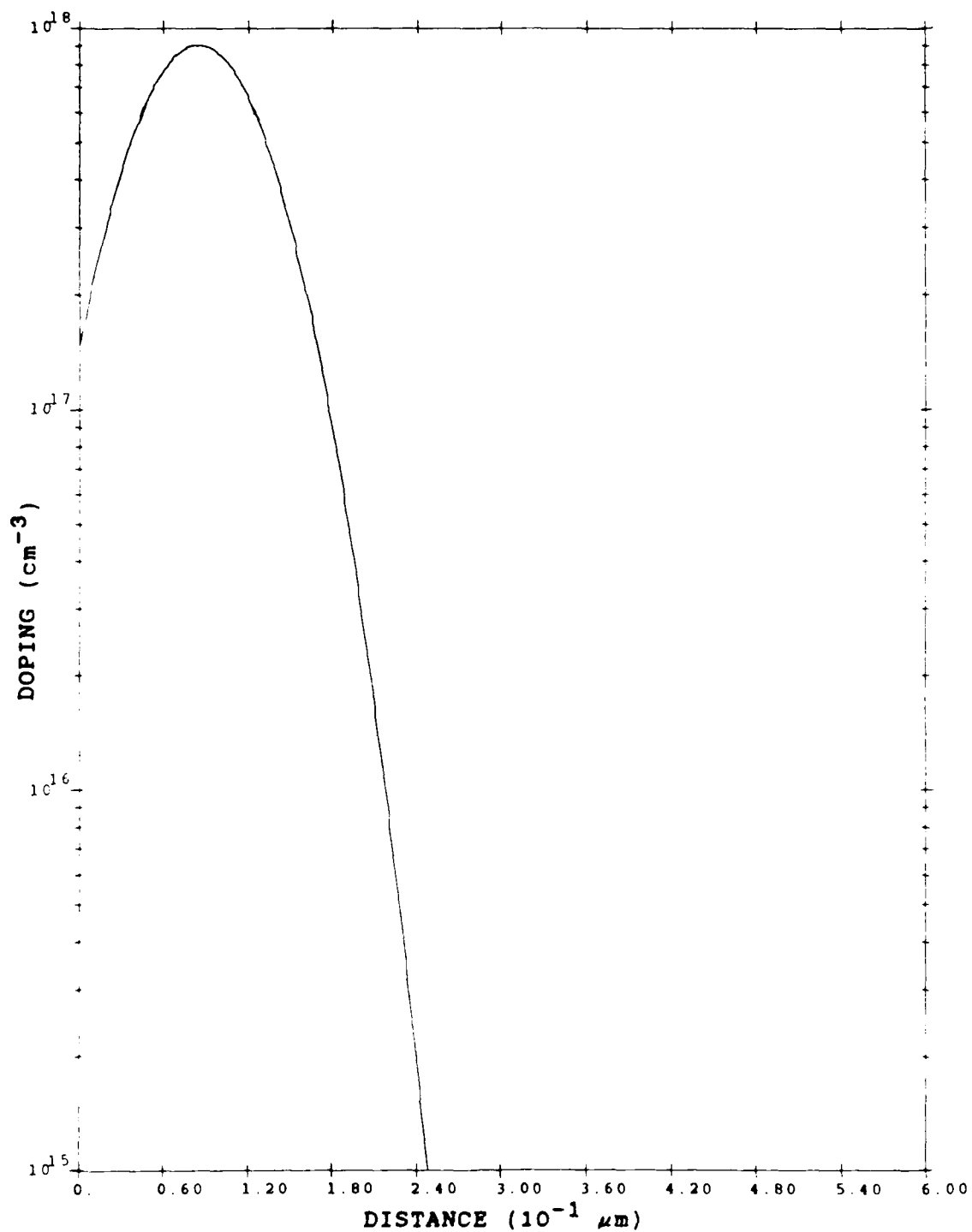


Figure 23. LSS Profile for Si-Implanted GaAs
 (Ion Dose: $1 \times 10^{13} \text{ cm}^{-2}$; Energy: 100 keV;
 Range: $.085 \mu\text{m}$; Standard Deviation: $.0442 \mu\text{m}$)

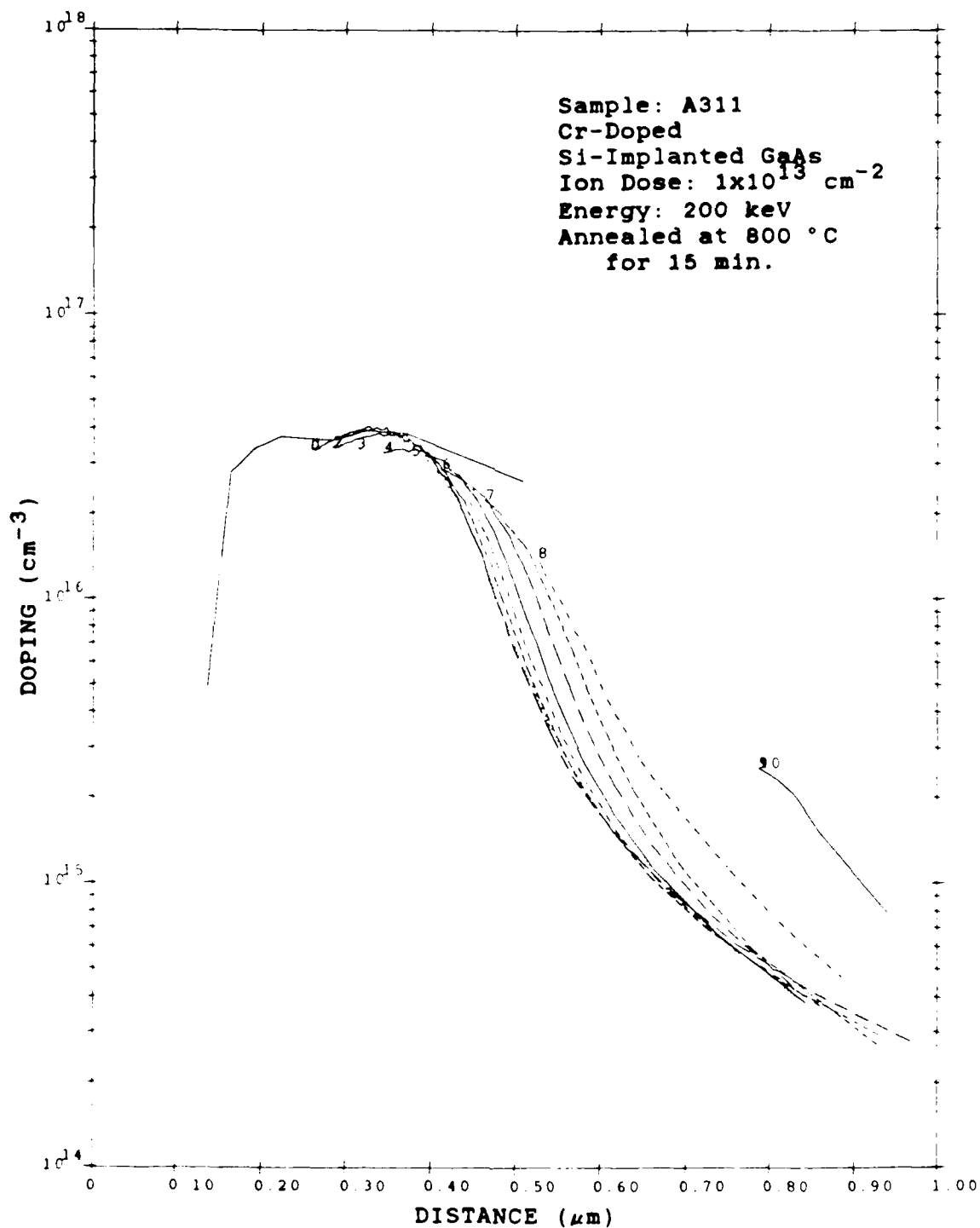


Figure 24. Performance of the Voltage First Derivative Method for Sample A311

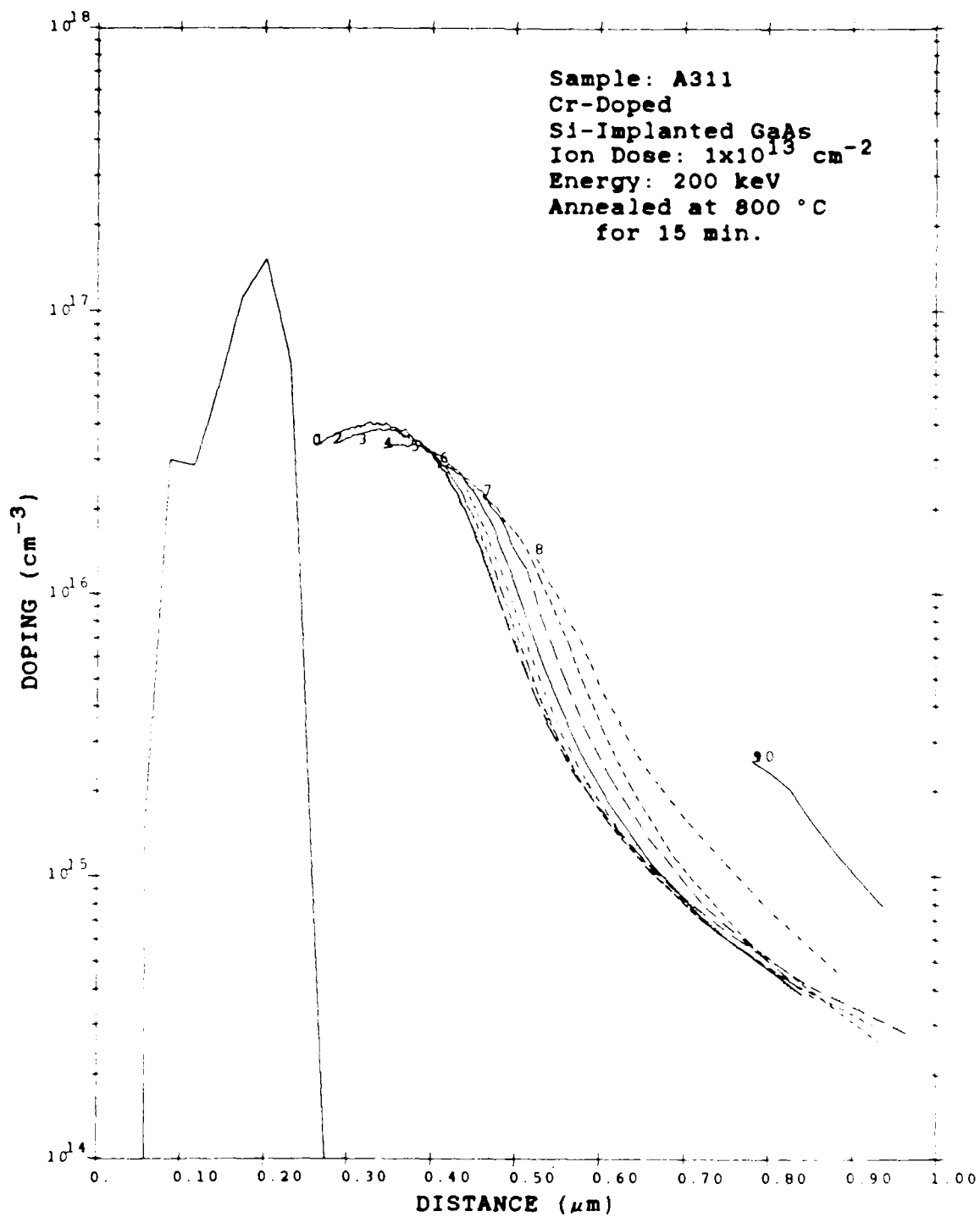


Figure 25. Performance of the Voltage Second Derivative Method for Sample A311 (Averaged Over the First 0.2 μm of Each C-V Profile)

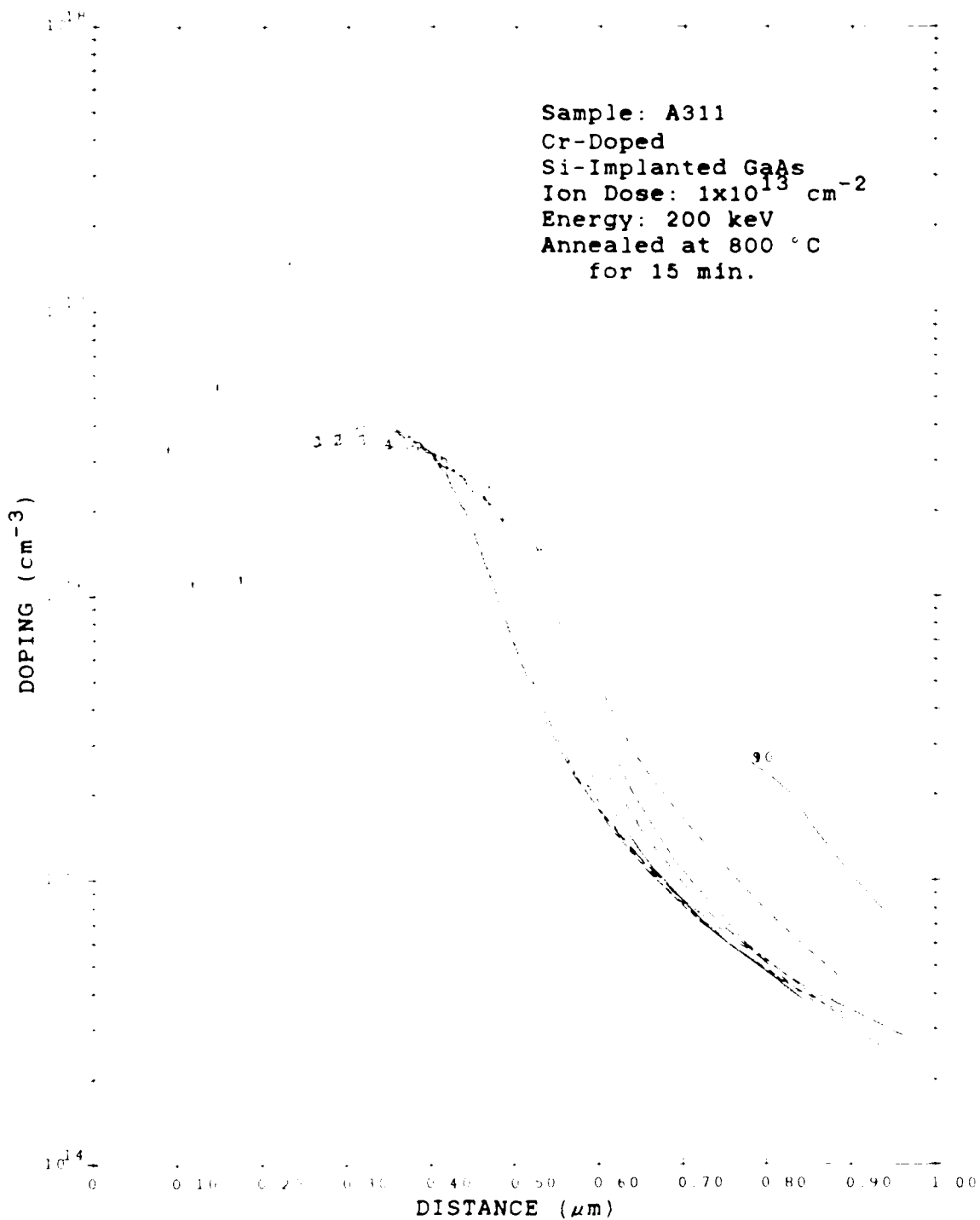


Figure 26. Performance of the Voltage Second Derivative Method for Sample A311 (Averaged Over the First 0.3 μm of Each C-V Profile)

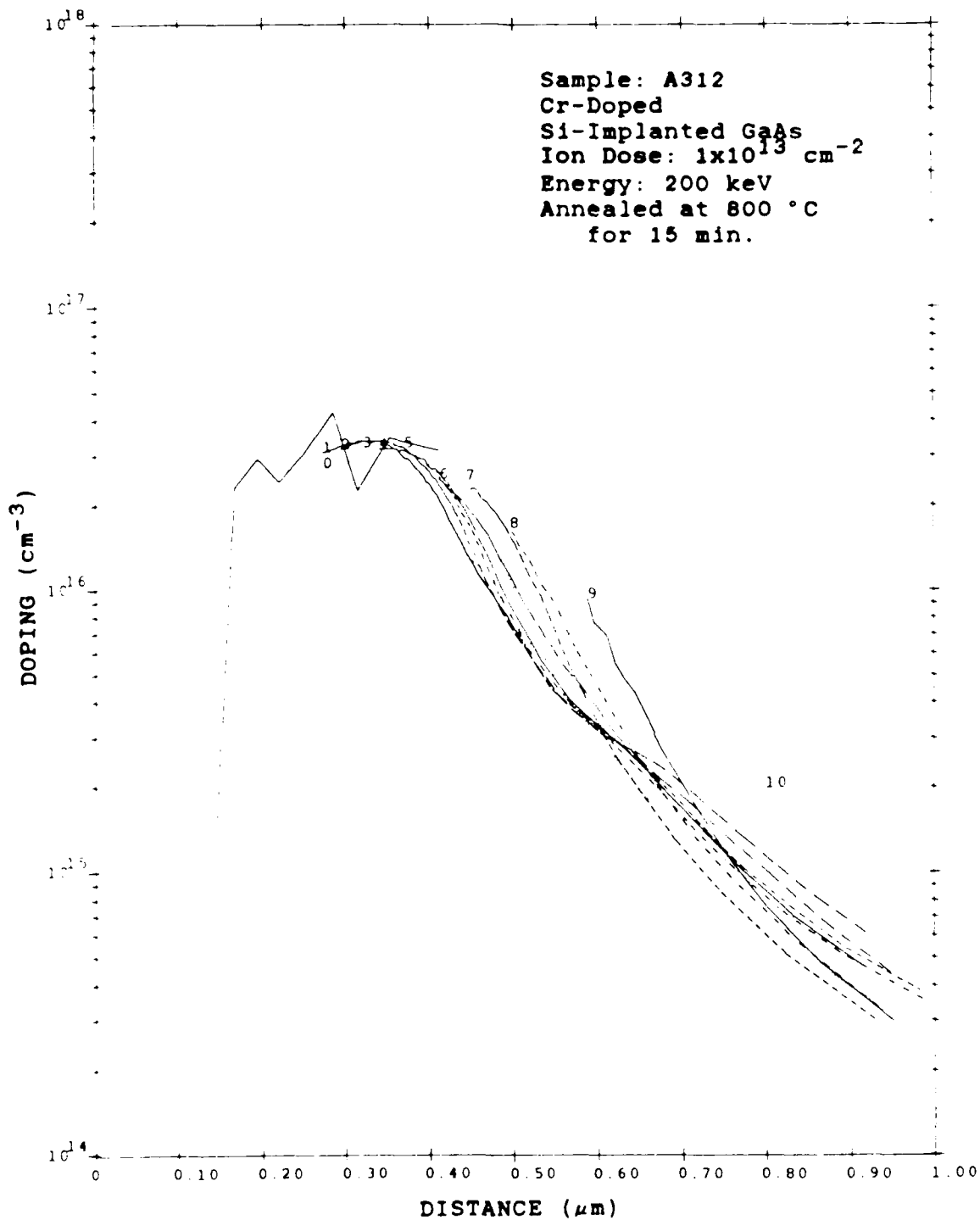


Figure 27. Performance of the Voltage First Derivative Method for Sample A312

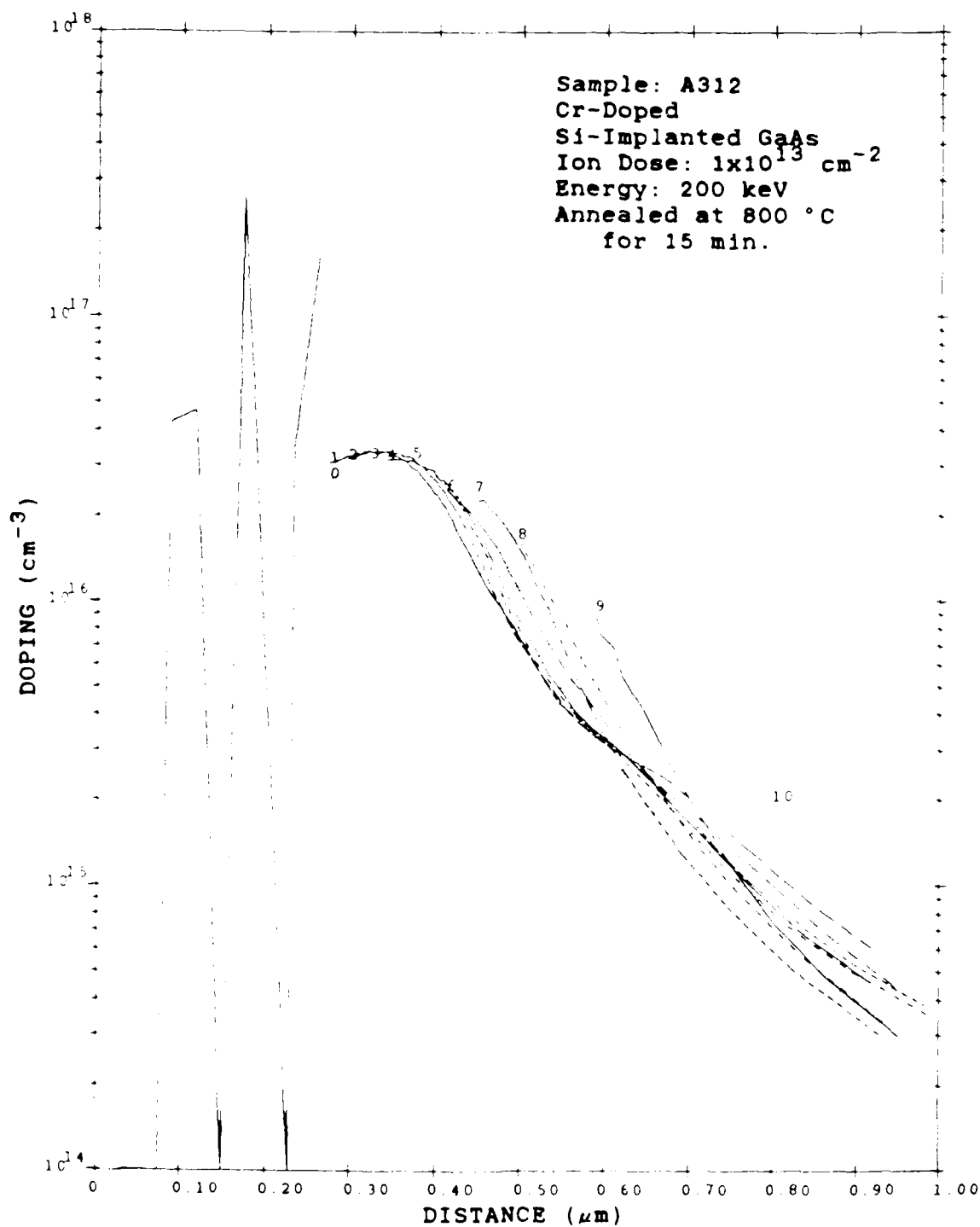


Figure 28. Performance of the Voltage Second Derivative Method for Sample A312 (Averaged Over the First 0.3 μm of Each C-V Profile)

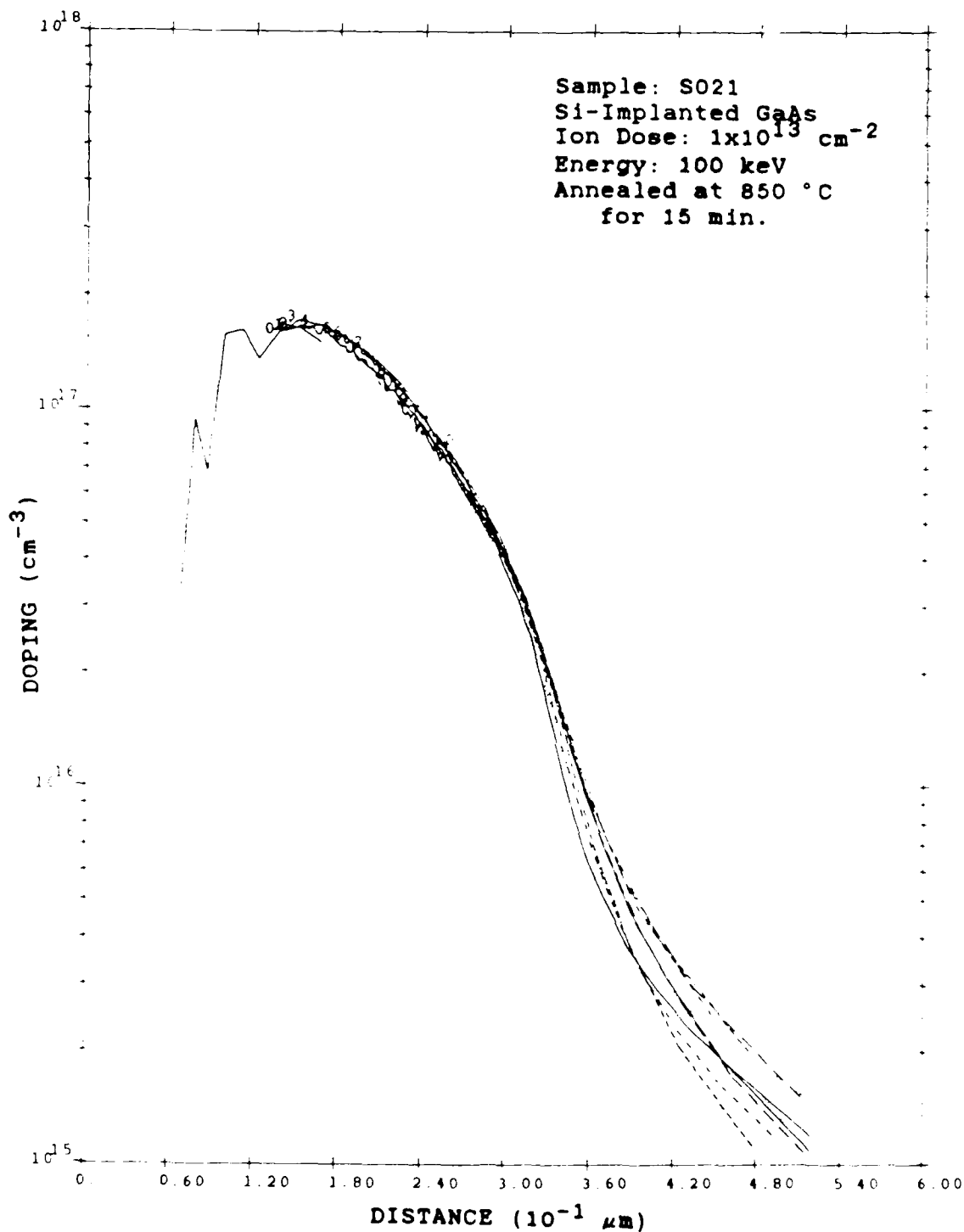


Figure 29. Performance of the Voltage First Derivative Method for Sample S021

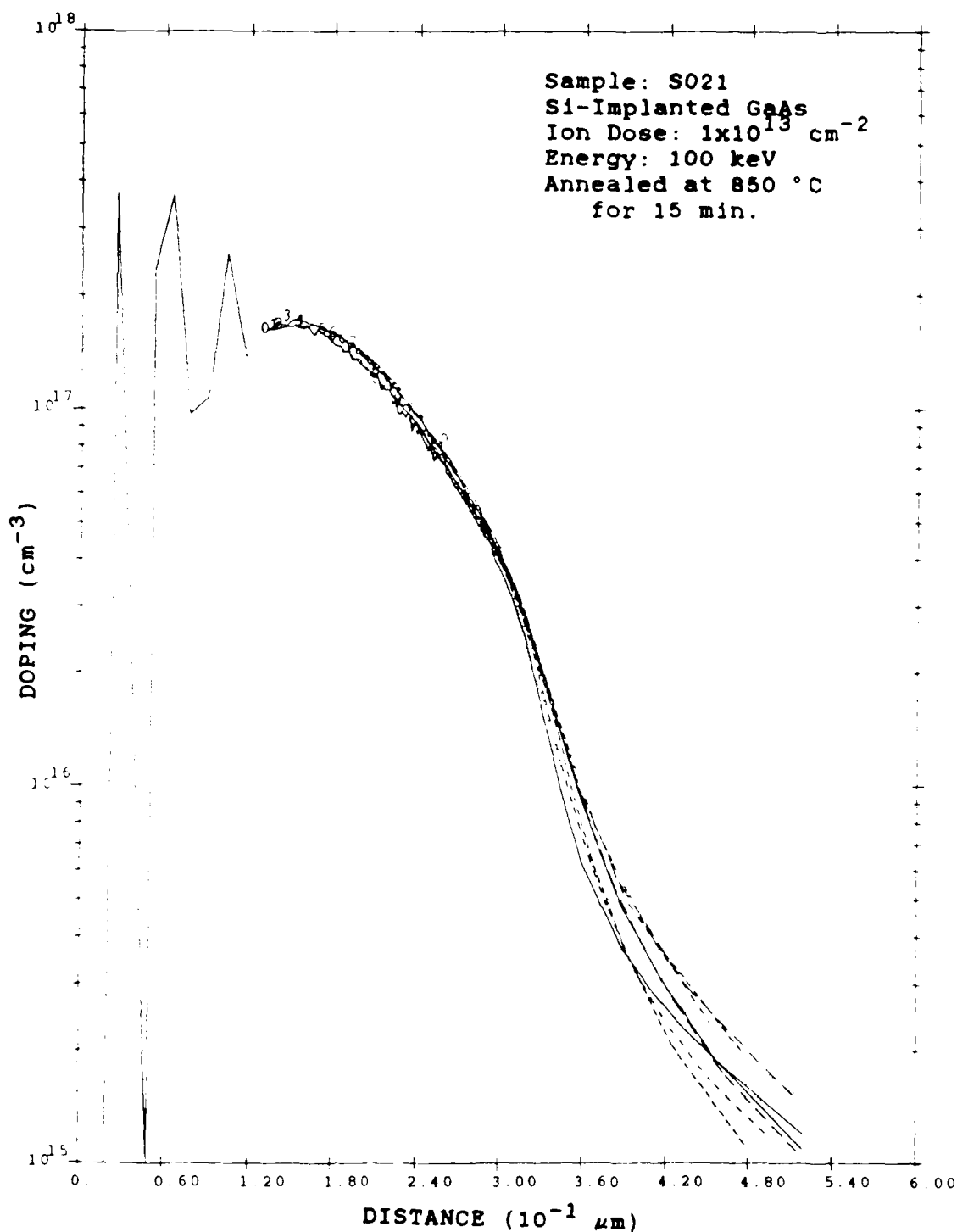


Figure 30. Performance of the Voltage Second Derivative Method for Sample S021 (Averaged Over the First $0.3 \mu\text{m}$ of Each C-V Profile)

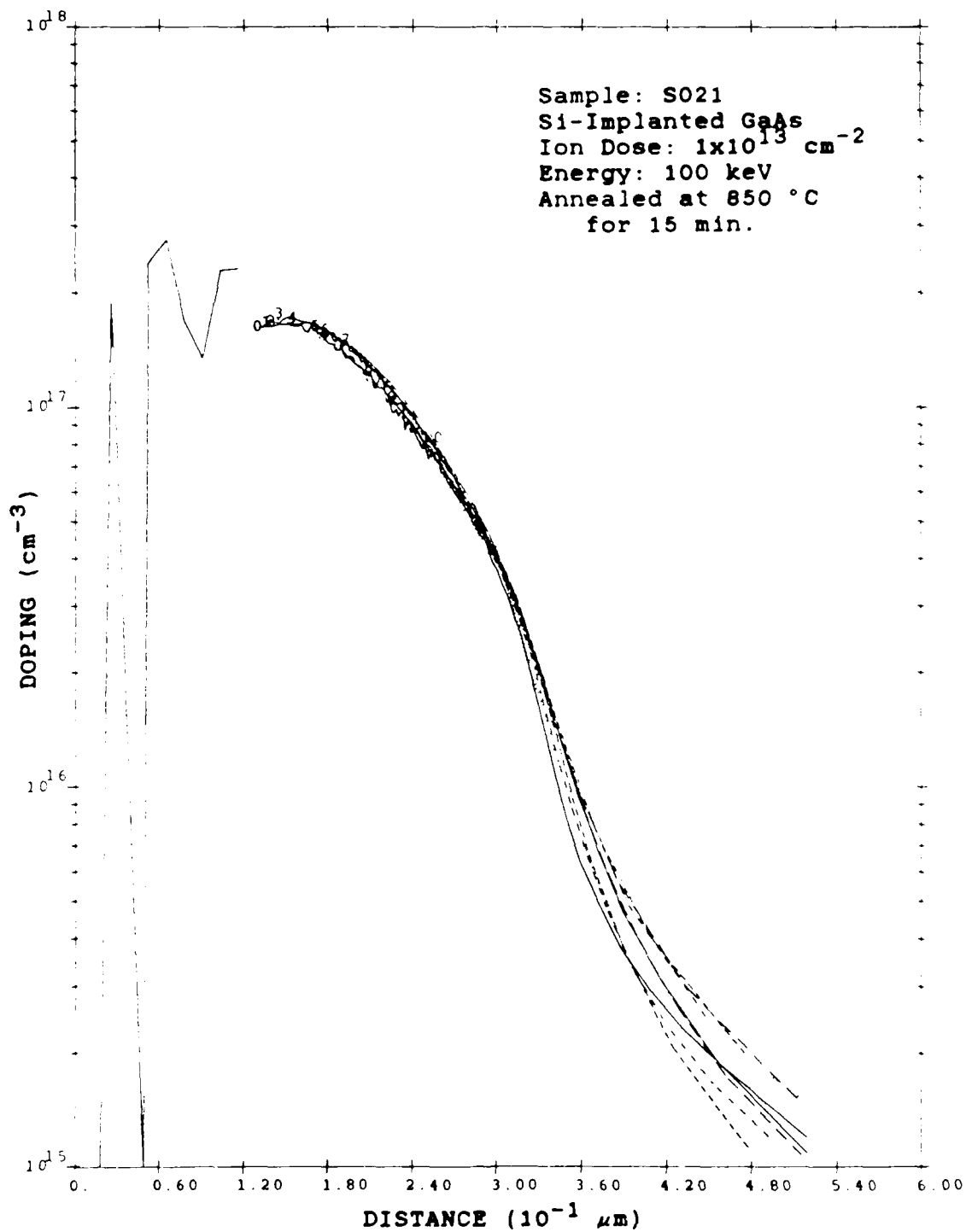


Figure 31. Performance of the Voltage Second Derivative Method for Sample S021 (Averaged Over a Range of $0.1 \mu\text{m}$ to $0.3 \mu\text{m}$ From the Start of Each C-V Profile)

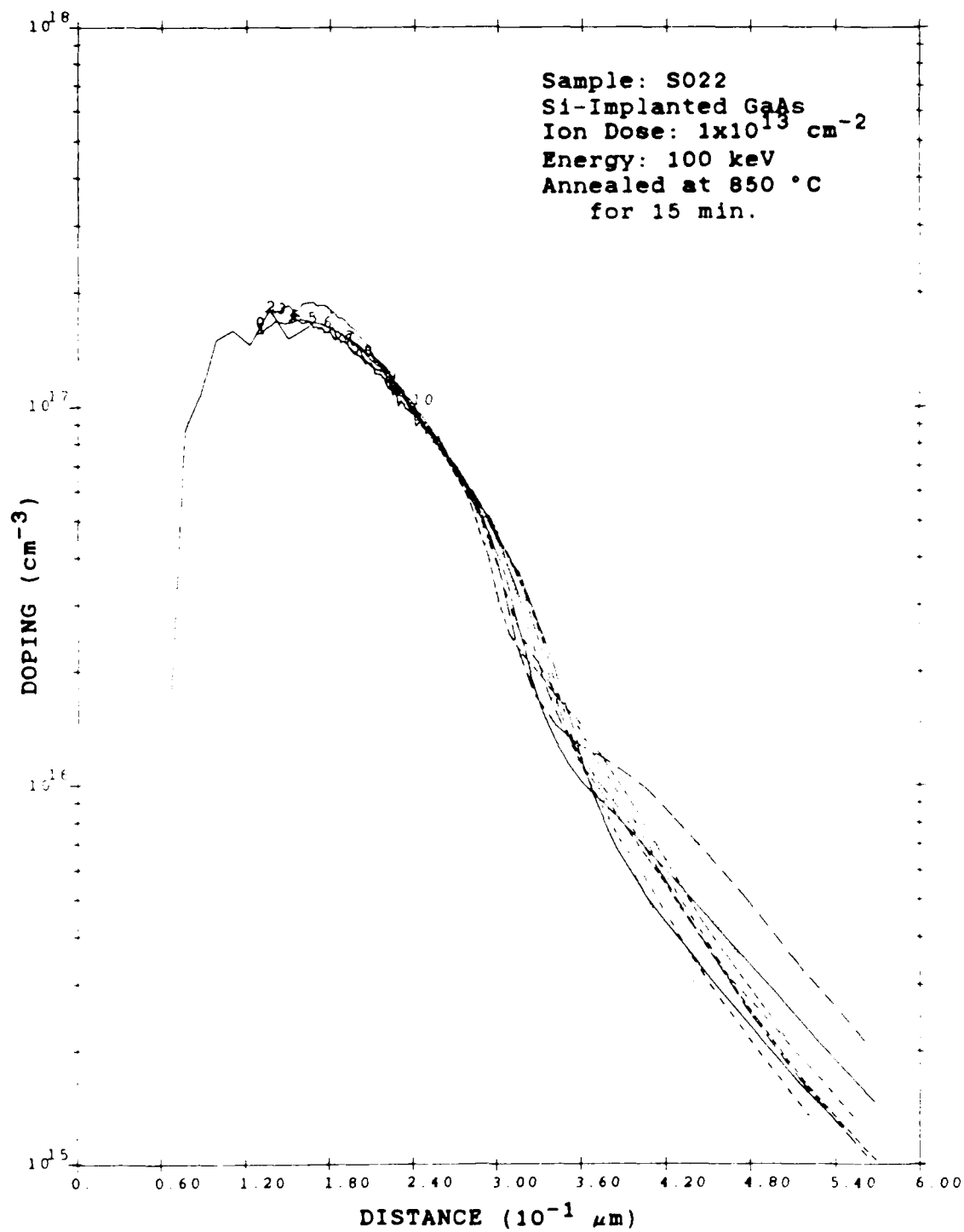


Figure 32. Performance of the Voltage First Derivative Method for Sample S022

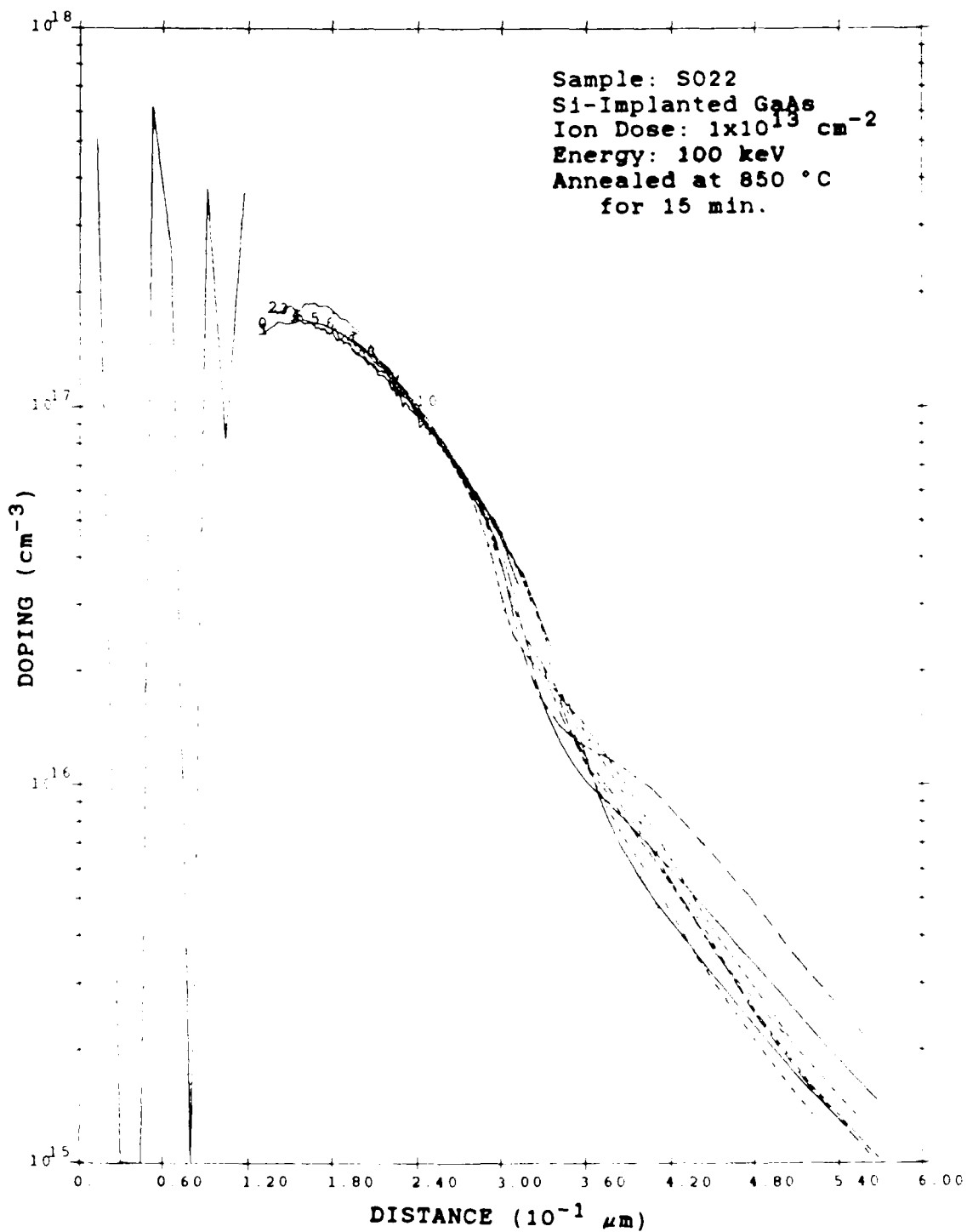


Figure 33. Performance of the Voltage Second Derivative Method for Sample S022 (Averaged Over a Range of 0.03 to 0.13 μm from the Start of Each C-V Profile)

VII. Conclusions and Recommendations

Conclusions

Methods were developed for finding the charge carrier concentrations within the initial depletion region of n-type semiconductors. These methods combine the capacitance-voltage (C-V) technique with the etching of layers from the semiconductor surface. After each etch, the depletion region is made to end at the same location within the semiconductor. This location is used as a common reference and is arbitrarily chosen at a distance deep below the original unetched surface. For each etch depth, the voltage which extends the depletion region to the common reference distance is found. The voltage drop from an etch depth to the deeper common reference distance is the same as it would be if the semiconductor was not etched. This voltage drop is the sum of the applied voltage and the built-in potential. The built-in potential depends on the barrier potential at the semiconductor surface and the concentration at the common reference distance. Assuming the barrier potential is the same for each etch surface, the built-in potential is constant for each etch. Consequently, the applied bias voltage at each etch surface, can be treated as the potential at that etch depth. Then equations, such as Poisson's equation, can be used to find the carrier concentrations within the initial depletion

region. These methods were successfully applied to ideal computer generated C-V data as well as experimental C-V measurements of Si-implanted GaAs.

Recommendations

Probably the main source of error in these methods is the fact that the depletion region ends gradually instead of abruptly. Wu et al. (22:319-329) showed how the shape of the depletion region changes with applied bias voltage for the regular C-V technique, and in a companion paper Klopfenstein and Wu (23:329-333) described computational methods for calculating the C-V measurements that would result from specified carrier distributions. These computational methods should be applied to check the accuracy of the methods developed in this thesis. The fact that the depletion region changes its shape should be less serious for the methods of this thesis than for the regular C-V technique, since a common reference distance is always used and each point in the depletion region should experience about the same potential regardless of whether material has been etched before it. If the common reference distance is far from the etch surfaces and the etch thicknesses are small, the basic shape of the depletion region should change little from one etch to the next. This is similar to an assumption for the regular C-V technique that the built-in potential changes little with increments in the applied bias voltage.

Another major source of error is oxidation of the semiconductor surface. The surface barrier height was assumed to remain constant for all the etch surfaces, but oxidation changes the barrier height. A change in the barrier height of 1 mV can very much change the concentration calculated. If the barrier height could be accurately measured for each etch surface, greater accuracy could be obtained and the methods could be simplified.

For greater accuracy, a much larger number of finer etches should be performed both within and outside the initial depletion region. Greater accuracy in the measurements of etch thicknesses, voltages, and capacitances would help. In this study, capacitances were measured to within 5, 4, and sometimes only 3 significant digits. The voltages may have been measured to within only 3 significant digits. The calculations were rather insensitive to inaccuracies in etch thicknesses, but the thicknesses were measured with an accuracy of about 10%.

Bibliography

1. Dearnaley, G. et al. Ion Implantation. Amsterdam: North-Holland Publishing Company, 1973.
2. Morgan, D.V. et al. "Prospects for Ion Bombardment and Ion Implantation in GaAs and InP Device Fabrication," IEE Proceedings, 128: 109-130, August 1981.
3. Stephens, K.G. and Sealy, B.J. "Use of ion implantation in future GaAs technology," Microelectronics, J.9: 13-18, 1978.
4. Yeo, Y.K., et al. "Surface-depletion effect correction to nonuniform carrier distributions by Hall measurements," Journal of Applied Physics, 61(11): 5070-5075, June 1987.
5. Gibbons, J.F. et al. "Projected Range Statistics: Semiconductors and Related Materials," Dowden, Hutchinson and Ross, Inc., 1975.
6. Carter, G. and Grant, W.A. "Ion Implantation of Semiconductors," Chap. 3, Edward Arnold, Ltd., London, 1976.
7. Chandra, A. et al. "Surface and Interface Depletion Corrections to Free Carrier Density Determinations by Hall Measurements," Solid State Electronics, 22, pp 645-650, December 1979.
8. Many, A. et al. Semiconductor Surfaces. Amsterdam: North-Holland Publishing Company, 1965.
9. Bardeen, J. "Surface States and Rectification at a Metal Semi-Conductor Contact," Physical Review, 71, pp 717-727, 1947.
10. McKelvey, J.P. Solid State and Semiconductor Physics. Malabar, Fla.: Robert & Krieger Publishing Co., 1966.
11. Shockley, W. "On the surface states associated with a periodic potential," Physical Review, 56, 317-323, August 1939.
12. Massies, J. et al. "Application of Molecular Beam Epitaxy to Study the Surface Properties of III-V Compounds," Proceedings of the 3rd International Conference on Solid Surfaces, pp 639-646, Vienna, 1977.

13. Henisch, H.K. Rectifying Semiconductor Contacts. Oxford: The Clarendon Press, 1957.
14. Schottky, W. "Verinfachte und Erweiterte Theorie der Randschichtgleichrichter," Zeitschrift fur Physik, 118, pp 539-592, September 1942.
15. Copeland, J.A. "A Technique for Directly Plotting the Inverse Doping Profile of Semiconductor Wafers," IEEE Transactions on Electron Devices, ED 16, No 5, pp 445-449, May 1969.
16. Miller, L. "A Feedback Method for Investigating Carrier Distributions in Semiconductors," IEEE Transactions on Electron Devices, ED 19, No 10, pp 1103-1198, October 1982.
17. Nakhamanson, R.S. "A Technique for Directly Plotting the Doping Profile of Semiconductor Wafers ('8-Shaped Way')," Solid State Electronics, 19, pp 84-89, 1976.
18. Sze, S.M. Physics of Semiconductor Devices, (2nd Ed.). Murray Hill, New Jersey: John Wiley & Sons, 1981.
19. Kim, Y.Y. Electrical Properties of Silicon-Implanted GaAs. MS Thesis. PH-82D-17. School of Engineering, Air Force Institute of Technology (AU), Wright-Patterson AFB, OH, December 1982.
20. Giacoletto, L. "Junction Capacitance and Related Characteristics Using Graded Impurity Semiconductors," IRE Transactions on Electron Devices, ED 4, pp 207-215, July 1957.
21. Norwood, H.M. et al. "Voltage Variable Capacitor Tuning: A Review," Proceedings of the IEEE, Vol 56, No 5, pp 788-798, May 1968.
22. Wu, C.P. et al. "Limitations of the CV Technique for Ion-Implanted Profiles," IEEE Transactions on Electron Devices, ED 22, No 6, pp 319-329, June 1975.
23. Klopfenstein, R.W. and Wu, C.P. "Computer Solution of One-Dimensional Poisson's Equation," IEEE Transactions on Electron Devices, ED 22, No 6, pp 329-333, June 1975.

VITA

Gordon H. Gainer, Jr. was born on 16 January 1960 in Newark, Ohio. He graduated from Heath High School in 1978 and then attended Ohio State University, from which he received a Bachelor of Science in Engineering Physics. He received a commission in the USAF through the Officer Training School. His first assignment was to the Aero Propulsion Laboratory, with a subsequent assignment to the Air Force Institute of Technology, both at Wright-Patterson AFB, Ohio. His next assignment in 1988 was to the Technical Operations Division of the Air Force Technical Applications Center at McClellan AFB, California.

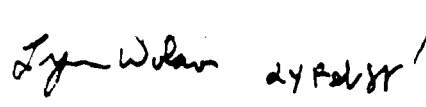
Permanent Address: 6300 Dundee Dr.
North Highlands CA 95660

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE

REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

1a REPORT SECURITY CLASSIFICATION UNCLASSIFIED			1b RESTRICTIVE MARKINGS	
2a SECURITY CLASSIFICATION AUTHORITY			3 DISTRIBUTION/AVAILABILITY OF REPORT Approved for public release; distribution unlimited.	
2b DECLASSIFICATION/DOWNGRADING SCHEDULE				
4 PERFORMING ORGANIZATION REPORT NUMBER(S) AFIT/GEP/ENP/87D-8			5 MONITORING ORGANIZATION REPORT NUMBER(S)	
6a NAME OF PERFORMING ORGANIZATION School of Engineering	6b OFFICE SYMBOL (If applicable) AFIT/ENP	7a NAME OF MONITORING ORGANIZATION		
6c ADDRESS (City, State, and ZIP Code) Air Force Institute of Technology (AU) Wright-Patterson AFB, Ohio 45433-6583		7b ADDRESS (City, State, and ZIP Code)		
8a NAME OF FUNDING SPONSORING ORGANIZATION	8b OFFICE SYMBOL (If applicable)	9 PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER		
8c ADDRESS (City, State, and ZIP Code)		10 SOURCE OF FUNDING NUMBERS		
		PROGRAM ELEMENT NO	PROJECT NO	TASK NO
		WORK UNIT ACCESSION NO		
11 TITLE (Include Security Classification) CALCULATING DEPLETION REGION CARRIER CONCENTRATIONS WITH CAPACITANCE-VOLTAGE MEASUREMENTS AND ETCHING (UNCLASSIFIED)				
12 PERSONAL AUTHOR(S) Gordon H. Gainer, Jr., Capt, USAF				
13a TYPE OF REPORT MS Thesis	13b TIME COVERED FROM _____ TO _____	14 DATE OF REPORT (Year, Month, Day) 1987 December	15 PAGE COUNT 79	
16 SUPPLEMENTARY NOTATION				
17 COSAT CODES			18 SUBJECT TERMS (Continue on reverse if necessary and identify by block number)	
FIELD	GROUP	SUB GROUP		
20	12		Surface Depletion, Depletion Region, Carrier Concentration Profiles, Ion Implantation, CAPACITANCE-VOLTAGE TECHNIQUE, C-V TECHNIQUE	
19 ABSTRACT (Continue on reverse if necessary and identify by block number)				
Title: CALCULATING DEPLETION REGION CARRIER CONCENTRATIONS WITH CAPACITANCE-VOLTAGE MEASUREMENTS AND ETCHING				
Thesis Chairman: Yung Kee Yeo, Ph.D. Professor of Physics				
				
20 DISTRIBUTION AVAILABILITY OF ABSTRACT <input checked="" type="checkbox"/> UNCLASSIFIED/UNLIMITED <input type="checkbox"/> SAME AS RPT <input type="checkbox"/> DTIC USERS			21 ABSTRACT SECURITY CLASSIFICATION UNCLASSIFIED	
22a NAME OF RESPONSIBLE INDIVIDUAL Yung Kee Yeo, Ph.D.			22b TELEPHONE (Include Area Code) 513-255-4498	22c OFFICE SYMBOL AFIT/ENP

Methods were developed for finding the charge carrier concentrations within the initial depletion region of n-type semiconductors. These methods combine the capacitance-voltage (C-V) technique with the etching of layers from the semiconductor surface. After each etch, the depletion region is made to end at the same location within the semiconductor. This location is used as a common reference and is arbitrarily chosen at a distance deep below the original unetched surface. For each etch depth, the voltage which extends the depletion region to the common reference distance is found. The voltage drop from an etch depth to the deeper common reference distance is the same as it would be if the semiconductor was not etched. This voltage drop is the sum of the applied voltage and the built-in potential. The built-in potential depends on the barrier potential at the semiconductor surface and the concentration at the common reference distance. Assuming the barrier potential is the same for each etch surface, the built-in potential is constant for each etch. Consequently, the applied bias voltage at each etch surface, can be treated as the potential at that etch depth. Then equations, such as Poisson's equation, can be used to find the carrier concentrations within the initial depletion region. These methods were successfully applied to ideal computer generated C-V data as well as experimental C-V measurements of Si-implanted GaAs.

END

DATE

FILMED

APRIL

1988

DTIC